



Vinyl ester styrene-free mortar anchor, for use in non-cracked concrete

MO-VSF

Assessed ETA Option 7 (non-cracked concrete).



PRODUCT INFORMATION

DESCRIPTION

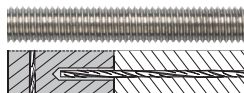
Vinyl ester styrene-free, chemical anchor.



OFFICIAL DOCUMENTATION

- ETA 24/0724 option 7, de M8 a M24 or non-cracked concrete.
- ETA 24/0726 or post-installed rebar installation.
- ETA 24/725 for installation in masonry.
- Certificate 1020-CPD-090-063589 for use in concrete.
- Certificate EVCP 1020-CPR-090-063593 for post-installed rebars.
- Certificate EVCP 1020-CPR-090-063591 for installation in masonry.
- Declaration features DoP MO-VSF.

VALID FOR



Stud



Post-installed rebar

DIMENSIONS

Stud M8 - M24

Post-installed rebars Ø8 - Ø16

RANGE OF CACULATION LOADS

From 7,8 to 48,3 kN (non-cracked).

BASE MATERIAL

Concrete quality C20/25 to C50/60 non-cracked.



Concrete

Hollow brick

Solid brick

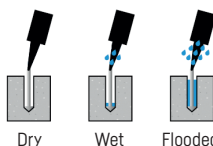
Thermal clay

ASSESSMENTS

- ETA 24/0724 Option 7: non-cracked concrete.
- ETA 24/0726 Post-installed rebars.
- ETA 24/0725 Masonry.



DRILL HOLE CONDITION



Dry

Wet

Flooded

CHARACTERISTICS AND BENEFITS

- Easy installation.
- For use in non-cracked concrete,
- Used for high loads.
- Temperature range -40°C to +80°C (maximum long-term temperature +50°C).
- Variety of lengths and diameters: M8-M24-assessed studs, flexible assembly.
- For static or quasi-static loads.
- Version in zinc plated steel, stainless steel A4.
- Available in INDEXcal.



MATERIALS

Standard stud:

Carbon steel 5.8, 8.8.



Stainless standard stud:

Stainless steel A2-70 and A4-70.



APPLICATIONS

- For indoor and outdoor use.
- Structural applications.
- Safety barriers.
- Fixing of road fences.
- Fixing of posters, machinery, boilers, signs, billboards, etc.





CONCRETE INSTALLATION PARAMETERS

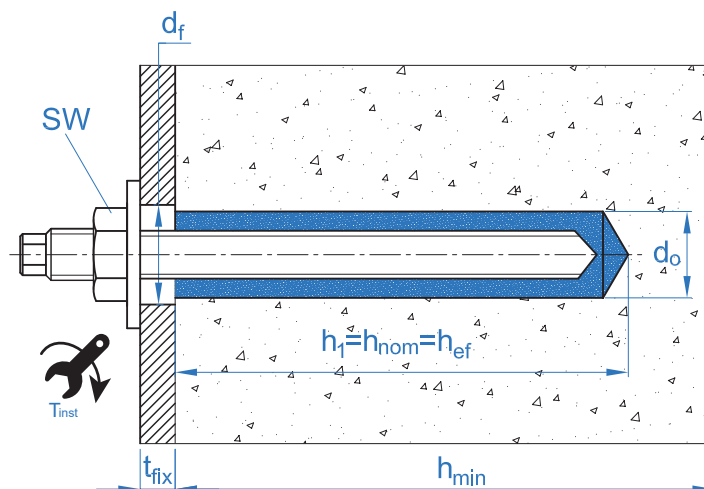
| METRIC | | | M8 | M10 | M12 | M16 | M20 | M24 |
|-------------------------|---------------------------------|------|-----|-----|-----|-----|-----|-----|
| d_0 | nominal diameter | [mm] | 10 | 12 | 14 | 18 | 22 | 26 |
| d_f | diameter in anchor plate \leq | [mm] | 9 | 12 | 14 | 18 | 22 | 26 |
| T_{inst} | tightening torque \leq | [Nm] | 10 | 20 | 40 | 80 | 150 | 200 |
| Circular cleaning brush | | | Ø14 | | Ø20 | | Ø29 | |

| $h_{ef,min} = 8d$ | | | | | | | | |
|-------------------|-----------------------------------|------|-----|-----|-----|-----|-----|-----|
| h_1 | depth of the drill hole | [mm] | 64 | 80 | 96 | 128 | 160 | 192 |
| $s_{cr,N}$ | critical distance between anchors | [mm] | 192 | 240 | 288 | 384 | 480 | 576 |
| $c_{cr,N}$ | critical distance from the edge | [mm] | 96 | 120 | 144 | 192 | 240 | 288 |
| c_{min} | minimum distance from the edge | [mm] | 35 | 40 | 50 | 65 | 80 | 96 |
| s_{min} | minimum distance between anchors | [mm] | 35 | 40 | 50 | 65 | 80 | 96 |
| h_{min} | minimum concrete thickness | [mm] | 100 | 110 | 126 | 158 | 204 | 244 |

| Standard stud | | | | | | | | |
|---------------|-----------------------------------|------|-----|-----|-----|-----|-----|-----|
| h_1 | depth of the drill hole | [mm] | 80 | 90 | 110 | 128 | 170 | 210 |
| $s_{cr,N}$ | critical distance between anchors | [mm] | 240 | 270 | 330 | 384 | 510 | 630 |
| $c_{cr,N}$ | critical distance from the edge | [mm] | 120 | 135 | 165 | 192 | 255 | 315 |
| c_{min} | minimum distance from the edge | [mm] | 43 | 45 | 56 | 65 | 85 | 105 |
| s_{min} | minimum distance between anchors | [mm] | 43 | 45 | 56 | 65 | 85 | 105 |
| h_{min} | minimum concrete thickness | [mm] | 110 | 120 | 140 | 158 | 214 | 262 |

| $h_{ef,max} = 12d$ | | | | | | | | |
|--------------------|-----------------------------------|------|-----|-----|-----|-----|-----|-----|
| h_1 | depth of the drill hole | [mm] | 96 | 120 | 144 | 192 | 240 | 288 |
| $s_{cr,N}$ | critical distance between anchors | [mm] | 288 | 360 | 432 | 576 | 720 | 864 |
| $c_{cr,N}$ | critical distance from the edge | [mm] | 144 | 180 | 216 | 288 | 360 | 432 |
| c_{min} | minimum distance from the edge | [mm] | 50 | 60 | 70 | 95 | 120 | 145 |
| s_{min} | minimum distance between anchors | [mm] | 50 | 60 | 70 | 95 | 120 | 145 |
| h_{min} | minimum concrete thickness | [mm] | 126 | 150 | 174 | 222 | 284 | 340 |

| | | | | | | |
|-----------------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|------------------------|
| Zinc-plated stud code 5.8 / 8.8 | EQAC08110 EQ8808110 | EQAC10130 EQ8810130 | EQAC12160 EQ8812160 | EQAC16190 EQ8816190 | EQAC20260 EQ8820260 | EQAC24300 EQ8824300 |
| Stainless steel stud code A2 / A4 | EQA208110 EQA408110 | EQA210130 EQA410130 | EQA212160 EQA412160 | EQA216190 EQA416190 | EQA220260 EQA420260 | EQA224300 EQA424300 |





| INSTALLATION ACCESSORIES | | | INSTALLATION PROCEDURE |
|-----------------------------------|------------------|--|------------------------|
| CODE | PRODUCT | MATERIAL | CONCRETE |
| MOPISSI | APPLICATION GUNS | Gun for 300 ml cartridges | |
| MOPISTO | | Guns for 410 ml cartridges, professional use | |
| MOPIISNEU | | Pneumatic gun for 410 ml coaxial cartridges, professional use | |
| EQ-AC EQ-8.8 EQ-A2 EQ-A4 | STUD | Studs threaded steel, class 5.8 ISO 898-1 Studs threaded steel, class 8.8 ISO 898-1 Studs stainless steel A2-70 Studs stainless steel A4-70 | |
| MORCEPKIT | CLEANING BRUSHES | Kit with 3 cleaning brushes measuring $\phi 14$, $\phi 20$ and $\phi 29$ mm | |
| MOBOMBA | CLEANING PUMP | Pump for cleaning leftover dust and fragments in the drill hole | |
| MORCANU | MIXING TUBE | Plastic. Static labyrinth mixture | |

| MINIMUM CURING TIME | | | | |
|---------------------|----------------------------|---------------------|--------------------------------|-------------------|
| TYPE | Cartridge temperature [°C] | Handling time [min] | Base material temperature [°C] | Curing time [min] |
| MO-VSF | min +5 | 18 | min +5 | 145 |
| | +5 a +10 | 10 | +5 a +10 | 145 |
| | +10 a +20 | 6 | +10 a +20 | 85 |
| | +20 a +25 | 5 | +20 a +25 | 50 |
| | +25 a +30 | 4 | +25 a +30 | 40 |
| | +30 | 4 | +30 | 35 |



Resistance in concrete C20/25 for an insulated anchor, without effects of distance from the edge or spacing between anchors, with a standard stud EQ-AC, EQ-8.8, EQ-A2 or EQ-A4

| Characteristic tensile strength N_{Rk} | | | | | | | | |
|--|----------------------|------|-------------|-------------|-------------|-------------|-------------|--------------|
| Metric | | | M8 | M10 | M12 | M16 | M20 | M24 |
| N_{Rk} | Non-cracked concrete | [kN] | 14,0 | 19,7 | 26,9 | 41,8 | 64,0 | 87,0 |
| Calculated tensile strength N_{Rd} | | | | | | | | |
| Metric | | | M8 | M10 | M12 | M16 | M20 | M24 |
| N_{Rd} | Non-cracked concrete | [kN] | 7,8 | 11,0 | 14,9 | 23,2 | 35,6 | 48,3 |
| Maximum recommended tensile load N_{rec} | | | | | | | | |
| Metric | | | M8 | M10 | M12 | M16 | M20 | M24 |
| N_{rec} | Non-cracked concrete | [kN] | 5,5 | 7,8 | 10,7 | 16,6 | 25,4 | 34,5 |
| Characteristic resistance to shear stress V_{Rk} | | | | | | | | |
| Metric | | | M8 | M10 | M12 | M16 | M20 | M24 |
| V_{Rk} | Zinc-plated stud | [kN] | <u>9,0</u> | <u>15,0</u> | <u>21,0</u> | <u>39,0</u> | <u>61,0</u> | <u>88,0</u> |
| | Stainless steel stud | [kN] | <u>13,0</u> | <u>20,0</u> | <u>30,0</u> | <u>55,0</u> | <u>86,0</u> | <u>124,0</u> |
| Calculated resistance to shearing V_{Rd} | | | | | | | | |
| Metric | | | M8 | M10 | M12 | M16 | M20 | M24 |
| V_{Rd} | Zinc-plated stud | [kN] | <u>7,2</u> | <u>12,0</u> | <u>16,8</u> | <u>31,2</u> | <u>48,8</u> | <u>70,4</u> |
| | Stainless steel stud | [kN] | <u>8,3</u> | <u>12,8</u> | <u>19,2</u> | <u>35,3</u> | <u>55,1</u> | <u>79,5</u> |
| Maximum recommended load to shear stress V_{rec} | | | | | | | | |
| Metric | | | M8 | M10 | M12 | M16 | M20 | M24 |
| V_{rec} | Zinc-plated stud | [kN] | <u>5,1</u> | <u>8,6</u> | <u>12,0</u> | <u>22,3</u> | <u>34,9</u> | <u>50,3</u> |
| | Stainless steel stud | [kN] | <u>6,0</u> | <u>9,2</u> | <u>13,7</u> | <u>25,2</u> | <u>39,4</u> | <u>56,8</u> |
| Effective depth of studs EQ-AC / EQ-A2 / EQ-A4 | | | | | | | | |
| Metric | | | M8 | M10 | M12 | M16 | M20 | M24 |
| Effective depth | | [mm] | 80 | 90 | 110 | 128 | 170 | 210 |

The values underlined and in italics indicate steel failure

Simplified calculation method. European Technical Assessment ETA 24/0724

Simplified version of the calculation method according to Eurocode 2 EN 1992-4. Resistance is calculated according to the data shown in assessment ETA 24/0724.

- Influence of concrete resistance.
- Influence of the distance from the edge of the concrete.
- Influence of the spacing between anchors.
- Influence of rebars.
- Influence of the base material thickness.
- Influence of the load application angle.
- Influence of the effective depth.
- Valid for a group of two anchors.
- Valid for dry or wet drill holes.

The calculation method is based on the following simplification:
No different loads act on individual anchors, without eccentricity.



INDEXcal

For a more precise calculation and taking into account more constructive arrangements we recommend the use of our INDEXcal calculation program. It can be downloaded free from our website www.indexfix.com

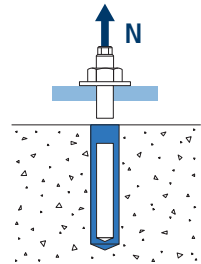


TENSILE LOADS

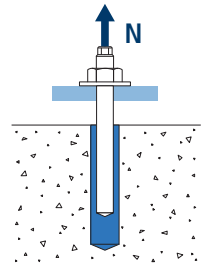
- Calculated steel resistance: $N_{Rd,s}$
- Calculated extraction resistance: $N_{Rd,p} = N_{Rd,p}^o \cdot \psi_c \cdot \psi_{hef,p}$
- Calculated concrete cone resistance: $N_{Rd,c} = N_{Rd,c}^o \cdot \psi_b \cdot \psi_{s,N} \cdot \psi_{c,N} \cdot \psi_{re,N} \cdot \psi_{hef,N}$
- Calculated concrete cracking resistance: $N_{Rd,sp} = N_{Rd,c}^o \cdot \psi_b \cdot \psi_{s,sp} \cdot \psi_{c,sp} \cdot \psi_{re,N} \cdot \psi_{h,sp} \cdot \psi_{hef,N}$

MO-VSF

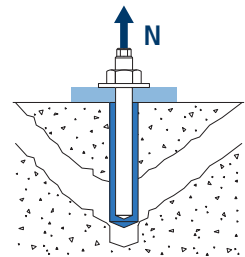
| Calculated steel resistance | | | | | | | |
|-----------------------------|------------------------------------|------|------|------|------|-------|-------|
| $N_{Rd,s}$ | | | | | | | |
| Metric | | M8 | M10 | M12 | M16 | M20 | M24 |
| $N_{Rd,s}^o$ | Steel class 5.8 | [kN] | 12,0 | 19,3 | 28,0 | 52,7 | 118,0 |
| | Steel class 8.8 | [kN] | 19,3 | 30,7 | 44,7 | 84,0 | 188,0 |
| | Steel class 10.9 | [kN] | 27,8 | 43,6 | 63,2 | 118,0 | 265,4 |
| | Stainless steel Class A2-70, A4-70 | [kN] | 13,9 | 21,9 | 31,6 | 58,8 | 92,0 |



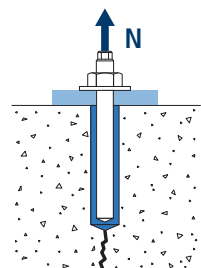
| Calculated extraction resistance | | | | | | | | |
|---|----------------------|------|-----|------|------|------|------|------|
| $N_{Rd,p} = N_{Rd,p}^o \cdot \psi_c \cdot \psi_{hef,p}$ | | | | | | | | |
| Metric | | M8 | M10 | M12 | M16 | M20 | M24 | |
| $N_{Rd,p}^o$ | Non-cracked concrete | [kN] | 7,8 | 11,0 | 15,0 | 23,2 | 35,6 | 48,4 |



| Calculated concrete cone resistance | | | | | | | | |
|---|----------------------|------|------|------|------|------|------|------|
| $N_{Rd,c} = N_{Rd,c}^o \cdot \psi_b \cdot \psi_{s,N} \cdot \psi_{c,N} \cdot \psi_{re,N} \cdot \psi_{hef,N}$ | | | | | | | | |
| Metric | | M8 | M10 | M12 | M16 | M20 | M24 | |
| $N_{Rd,c}^o$ | Non-cracked concrete | [kN] | 19,6 | 23,3 | 31,5 | 39,6 | 60,6 | 83,2 |



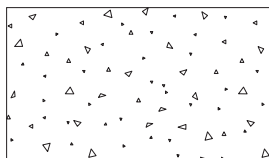
| Calculated concrete cracking resistance | | | | | | | | |
|--|----------------------|------|------|------|------|------|------|------|
| $N_{Rd,sp} = N_{Rd,c}^o \cdot \psi_b \cdot \psi_{s,sp} \cdot \psi_{c,sp} \cdot \psi_{re,N} \cdot \psi_{h,sp} \cdot \psi_{hef,N}$ | | | | | | | | |
| Metric | | M8 | M10 | M12 | M16 | M20 | M24 | |
| $N_{Rd,sp}^o$ | Non-cracked concrete | [kN] | 19,6 | 23,3 | 31,5 | 39,6 | 60,6 | 83,2 |





MO-VSF

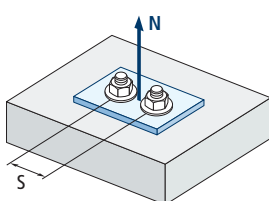
Influence coefficients



| Influence of concrete resistance for extraction Ψ_c | | | | | |
|--|----------------------|--------|--------|--------|--------|
| Concrete type | | C20/25 | C30/37 | C40/50 | C50/60 |
| Ψ_c | Non-cracked concrete | 1,00 | 1,10 | 1,18 | 1,25 |

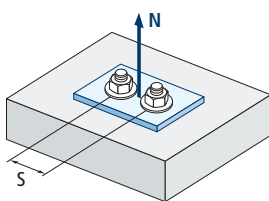
$$\Psi_b = \sqrt{\frac{f_{ck,cube}}{25}} \geq 1$$

| Influence of concrete resistance for concrete cone and concrete cracking Ψ_b | | | | | |
|---|--|--------|--------|--------|--------|
| Concrete type | | C20/25 | C30/37 | C40/50 | C50/60 |
| Ψ_b | | 1,00 | 1,22 | 1,41 | 1,55 |



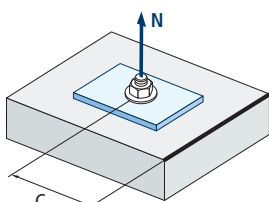
| Influence of spacing between anchors (concrete cone) $\Psi_{s,N}$ | | | | | | | | | | |
|---|------|------|------|------|------|------|------|------|------|------|
| $s/s_{cr,N}$ | 0,1 | 0,2 | 0,3 | 0,4 | 0,5 | 0,6 | 0,7 | 0,8 | 0,9 | 1,0 |
| $\Psi_{s,N}$ | 0,55 | 0,60 | 0,65 | 0,70 | 0,75 | 0,80 | 0,85 | 0,90 | 0,95 | 1,00 |

$$\Psi_{s,N} = 0,5 \left(1 + \frac{s}{s_{cr,N}} \right) \leq 1$$



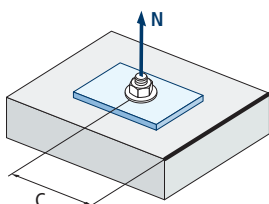
| Influence of spacing between anchors (cracking) $\Psi_{s,sp}$ | | | | | | | | | | |
|---|------|------|------|------|------|------|------|------|------|------|
| $s/s_{cr,sp}$ | 0,1 | 0,2 | 0,3 | 0,4 | 0,5 | 0,6 | 0,7 | 0,8 | 0,9 | 1,0 |
| $\Psi_{s,sp}$ | 0,55 | 0,60 | 0,65 | 0,70 | 0,75 | 0,80 | 0,85 | 0,90 | 0,95 | 1,00 |

$$\Psi_{s,sp} = 0,5 \left(1 + \frac{s}{s_{cr,sp}} \right) \leq 1$$



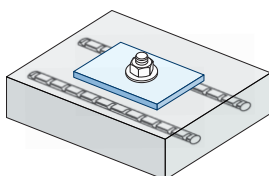
| Influence of the distance from the edge of the concrete (concrete cone) $\Psi_{c,N}$ | | | | | | | | | | | | |
|--|------|------|------|------|------|------|------|------|------|------|------|------|
| $c/C_{cr,N}$ | 0,1 | 0,2 | 0,3 | 0,5 | 0,6 | 0,8 | 0,9 | 1,1 | 1,2 | 1,4 | 1,5 | 1,6 |
| $\Psi_{c,N}$ | 0,40 | 0,46 | 0,51 | 0,45 | 0,49 | 0,55 | 0,61 | 0,67 | 0,75 | 0,83 | 0,91 | 1,00 |

$$\Psi_{c,N} = 0,35 + \frac{0,5 \cdot c}{C_{cr,N}} + \frac{0,15 \cdot c^2}{C_{cr,N}^2} \leq 1$$



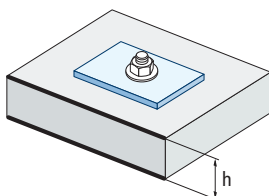
| Influence of the distance from the edge of the concrete (cracking) $\Psi_{c,sp}$ | | | | | | | | | | | | |
|--|------|------|------|------|------|------|------|------|------|------|------|------|
| $c/C_{cr,sp}$ | 0,1 | 0,2 | 0,3 | 0,5 | 0,6 | 0,8 | 0,9 | 1,1 | 1,2 | 1,4 | 1,5 | 1,6 |
| $\Psi_{c,sp}$ | 0,40 | 0,46 | 0,51 | 0,45 | 0,49 | 0,55 | 0,61 | 0,67 | 0,75 | 0,83 | 0,91 | 1,00 |

$$\Psi_{c,sp} = 0,35 + \frac{0,5 \cdot c}{C_{cr,sp}} + \frac{0,15 \cdot c^2}{C_{cr,sp}^2} \leq 1$$



| Influence of the rebars $\Psi_{re,N}$ | | | | | |
|---------------------------------------|------|------|------|------|------|
| h_{ef} (mm) | 64 | 70 | 80 | 90 | 100 |
| $\Psi_{re,N}$ | 0,82 | 0,85 | 0,90 | 0,95 | 1,00 |

$$\Psi_{re,N} = 0,5 + \frac{h_{ef}}{200} \leq 1$$



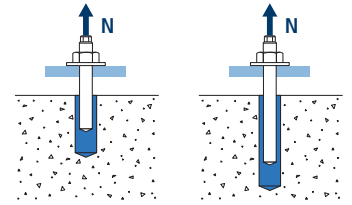
| Influence of the base material thickness $\Psi_{h,sp}$ | | | | | | | | | | | |
|--|------------|------|------|------|------|------|------|------|------|------|------|
| $\Psi_{h,sp}$ | h/h_{ef} | 2,00 | 2,20 | 2,40 | 2,60 | 2,80 | 3,00 | 3,20 | 3,40 | 3,60 | 3,68 |
| | fh | 1,00 | 1,07 | 1,13 | 1,19 | 1,25 | 1,31 | 1,37 | 1,42 | 1,48 | 1,50 |

$$\Psi_{h,sp} = \left(\frac{h}{2 \cdot h_{ef}} \right)^{2/3} \leq 1,5$$



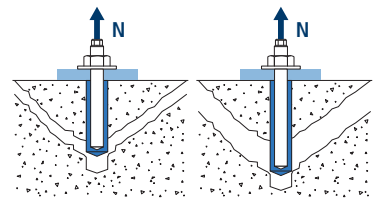
MO-VSF

| Influence of the effective depth for the extraction combination $\Psi_{hef,p}$ | | | | | | |
|--|------|------|------|------|------|------|
| Metric h_{ef} | M8 | M10 | M12 | M16 | M20 | M24 |
| 64 | 0,80 | | | | | |
| 80 | 1,00 | 0,89 | | | | |
| 90 | 1,13 | 1,00 | 0,82 | | | |
| 96 | 1,20 | 1,07 | 0,87 | | | |
| 110 | | 1,22 | 1,00 | | | |
| 120 | | 1,33 | 1,09 | | | |
| 128 | | | 1,16 | 1,00 | | |
| 144 | | | 1,31 | 1,13 | | |
| 160 | | | | 1,25 | 0,94 | |
| 170 | | | | 1,33 | 1,00 | |
| 192 | | | | 1,50 | 1,13 | 0,91 |
| 210 | | | | | 1,24 | 1,00 |
| 240 | | | | | 1,41 | 1,14 |
| 288 | | | | | | 1,37 |



$$\Psi_{hef,p} = \frac{h_{ef}}{h_{stand}}$$

| Influence of the effective depth for the concrete cone $\Psi_{hef,N}$ | | | | | | |
|---|------|------|------|------|------|------|
| Metric h_{ef} | M8 | M10 | M12 | M16 | M20 | M24 |
| 64 | 0,72 | | | | | |
| 80 | 1,00 | 0,84 | | | | |
| 90 | 1,19 | 1,00 | | | | |
| 96 | 1,31 | 1,10 | 0,82 | | | |
| 110 | 1,61 | 1,35 | 1,00 | | | |
| 120 | 1,84 | 1,54 | 1,14 | 0,91 | | |
| 128 | 2,02 | 1,70 | 1,26 | 1,00 | 0,65 | |
| 144 | | 2,02 | 1,50 | 1,19 | 0,78 | |
| 160 | | 2,37 | 1,75 | 1,40 | 0,91 | 0,67 |
| 170 | | 2,60 | 1,92 | 1,53 | 1,00 | 0,73 |
| 192 | | | 2,31 | 1,84 | 1,20 | 0,87 |
| 210 | | | 2,64 | 2,10 | 1,37 | 1,00 |
| 240 | | | 3,22 | 2,57 | 1,68 | 1,22 |
| 288 | | | | 3,38 | 2,21 | 1,61 |



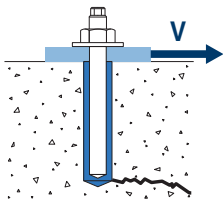
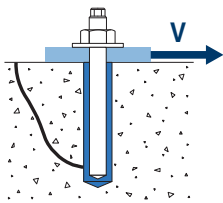
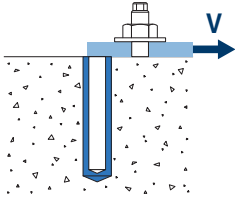
$$\Psi_{hef,N} = \left(\frac{h_{ef}}{h_{stand}} \right)^{1,5}$$



MO-VSF

SHEARING LOADS

- Calculated steel resistance without lever arm: $V_{Rd,s}$
- Calculated spalling resistance: $V_{Rd,cp} = k \cdot N_{Rd,c}^{\circ}$
- Calculated concrete edge resistance: $V_{Rd,c} = V_{Rd,c}^{\circ} \cdot \Psi_b \cdot \Psi_{se,V} \cdot \Psi_{c,V} \cdot \Psi_{re,V} \cdot \Psi_{\alpha,V} \cdot \Psi_{h,V}$



Calculated steel resistance to shearing

| | | $V_{Rd,s}$ | | | | | | |
|--------------------|------------------------------------|------------|-----|------|------|------|------|-------|
| Metric | | M8 | M10 | M12 | M16 | M20 | M24 | |
| $V_{Rd,s}^{\circ}$ | Steel class 5.8 | [kN] | 7,2 | 12 | 16,8 | 31,2 | 48,8 | 70,4 |
| | Steel class 8.8 | [kN] | 12 | 18,4 | 27,2 | 50,4 | 78,4 | 112,8 |
| | Steel class 10.9 | [kN] | 12 | 19,3 | 28 | 52,7 | 82 | 118 |
| | Stainless steel Class A2-70, A4-70 | [kN] | 8,3 | 12,8 | 19,2 | 35,3 | 55,1 | 79,5 |

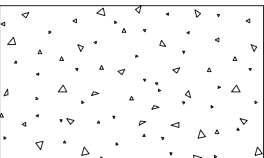
Calculated spalling resistance

| | | $V_{Rd,cp} = k \cdot N_{Rd,c}^{\circ}$ | | | | | |
|--------|--|--|-----|-----|-----|-----|-----|
| Metric | | M8 | M10 | M12 | M16 | M20 | M24 |
| k | | 2 | | | | | |

Calculated concrete edge resistance

| | | $V_{Rd,c} = V_{Rd,c}^{\circ} \cdot \Psi_b \cdot \Psi_{se,V} \cdot \Psi_{c,V} \cdot \Psi_{re,V} \cdot \Psi_{\alpha,V} \cdot \Psi_{h,V}$ | | | | | | |
|--------------------|----------------------|--|-----|-----|------|------|------|------|
| Metric | | M8 | M10 | M12 | M16 | M20 | M24 | |
| $V_{Rd,c}^{\circ}$ | Non-cracked concrete | [kN] | 5,7 | 8,6 | 11,8 | 19,0 | 28,3 | 36,4 |

Influence coefficients

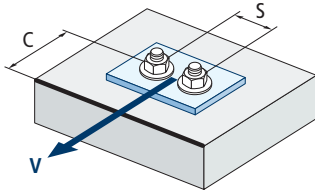
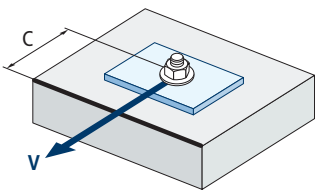


$$\Psi_b = \sqrt{\frac{f_{ck,cube}}{25}} \geq 1$$

| Influence of concrete resistance for concrete cone and concrete cracking Ψ_b | | | | |
|---|--------|--------|--------|--------|
| Concrete type | C20/25 | C30/37 | C40/50 | C50/60 |
| Ψ_b | 1,00 | 1,22 | 1,41 | 1,55 |

Influence of the distance from the edge and spacing between anchors $\Psi_{se,V}$

| For one anchor | | | | | | | | | | | | | | | | | |
|-----------------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|-------|
| c/h_{ef} | 0,50 | 0,75 | 1,00 | 1,25 | 1,50 | 1,75 | 2,00 | 2,25 | 2,50 | 2,75 | 3,00 | 3,25 | 3,50 | 3,75 | 4,00 | 4,50 | 5,00 |
| Insulated | 0,35 | 0,65 | 1,00 | 1,40 | 1,84 | 2,32 | 2,83 | 3,38 | 3,95 | 4,56 | 5,20 | 5,86 | 6,55 | 7,26 | 8,00 | 9,55 | 11,18 |
| For two anchors | | | | | | | | | | | | | | | | | |
| c/h_{ef} | 0,50 | 0,75 | 1,00 | 1,25 | 1,50 | 1,75 | 2,00 | 2,25 | 2,50 | 2,75 | 3,00 | 3,25 | 3,50 | 3,75 | 4,00 | 4,50 | 5,00 |
| 1,0 | 0,24 | 0,43 | 0,67 | 0,93 | 1,22 | 1,54 | 1,89 | 2,25 | 2,64 | 3,04 | 3,46 | 3,91 | 4,37 | 4,84 | 5,33 | 6,36 | 7,45 |
| 1,5 | 0,27 | 0,49 | 0,75 | 1,05 | 1,38 | 1,74 | 2,12 | 2,53 | 2,96 | 3,42 | 3,90 | 4,39 | 4,91 | 5,45 | 6,00 | 7,16 | 8,39 |
| 2,0 | 0,29 | 0,54 | 0,83 | 1,16 | 1,53 | 1,93 | 2,36 | 2,81 | 3,29 | 3,80 | 4,33 | 4,88 | 5,46 | 6,05 | 6,67 | 7,95 | 9,32 |
| 2,5 | 0,32 | 0,60 | 0,92 | 1,28 | 1,68 | 2,12 | 2,59 | 3,09 | 3,62 | 4,18 | 4,76 | 5,37 | 6,00 | 6,66 | 7,33 | 8,75 | 10,25 |
| $\geq 3,0$ | 0,35 | 0,65 | 1,00 | 1,40 | 1,84 | 2,32 | 2,83 | 3,38 | 3,95 | 4,56 | 5,20 | 5,86 | 6,55 | 7,26 | 8,00 | 9,55 | 11,18 |



$$\Psi_{se,V} = \left(\frac{c}{h_{ef}}\right)^{1,5}$$

$$\Psi_{se,V} = \left(\frac{c}{h_{ef}}\right)^{1,5} \cdot \left(1 + \frac{s}{3 \cdot c}\right) \cdot 0,5 \leq \left(\frac{c}{h_{ef}}\right)^{1,5}$$

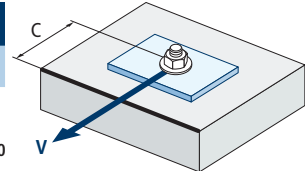


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Influence of the distance from the edge of the concrete $\Psi_{c,v}$

| c/d | 4 | 5 | 7 | 10 | 15 | 20 | 25 | 30 |
|--------------|------|------|------|------|------|------|------|------|
| $\Psi_{c,v}$ | 0,76 | 0,72 | 0,68 | 0,63 | 0,58 | 0,55 | 0,53 | 0,51 |

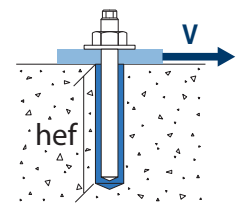
$$\Psi_{c,v} = \left(\frac{d}{c}\right)^{0,20}$$



Influence of the effective depth $\Psi_{hef,v}$

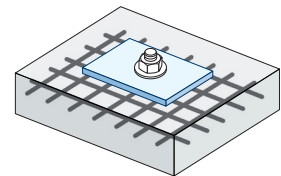
| h_{ef}/d | 8 | 9 | 10 | 11 | 12 |
|----------------|------|------|------|------|------|
| $\Psi_{hef,v}$ | 1,65 | 2,04 | 2,47 | 2,93 | 3,42 |

$$\Psi_{hef,v} = 0,04 \cdot \left(\frac{h_{ef}}{d}\right)^{1,79}$$



Influence of the rebars $\Psi_{re,v}$

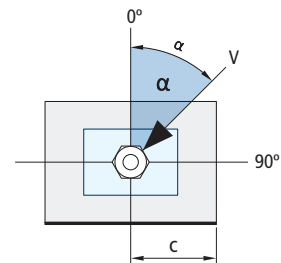
| $\Psi_{re,v}$ | Non-cracked concrete | Without perimeter rebar | Perimeter rebar $\geq \varnothing 12\text{mm}$ | Perimeter rebar with abutments at $\leq 100\text{mm}$ |
|---------------|----------------------|-------------------------|--|---|
| | | 1 | 1 | 1 |



Influence of the load application angle $\Psi_{\alpha,v}$

| Angle, α (°) | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 90° |
|---------------------|------|------|------|------|------|------|------|------|------|------|
| $\Psi_{\alpha,v}$ | 1,00 | 1,01 | 1,05 | 1,13 | 1,24 | 1,40 | 1,64 | 1,97 | 2,32 | 2,50 |

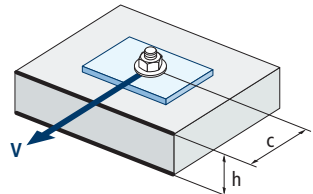
$$\Psi_{\alpha,v} = \sqrt{\frac{1}{(\cos \alpha_v)^2 + \left(\frac{\sin \alpha_v}{2,5}\right)^2}} \geq 1$$



Influence of the base material thickness $\Psi_{h,v}$

| h/c | 0,15 | 0,30 | 0,45 | 0,60 | 0,75 | 0,90 | 1,05 | 1,20 | 1,35 | $\geq 1,5$ |
|--------------|------|------|------|------|------|------|------|------|------|------------|
| $\Psi_{h,v}$ | 0,32 | 0,45 | 0,55 | 0,63 | 0,71 | 0,77 | 0,84 | 0,89 | 0,95 | 1,00 |

$$\Psi_{h,v} = \left(\frac{h}{1,5 \cdot c}\right)^{0,5} \geq 1,0$$



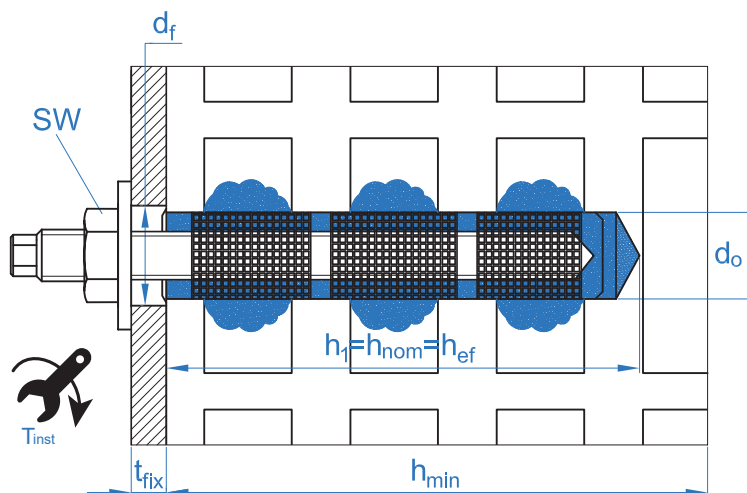


MO-VSF

FIXING IN BRICKS

| MO-VSF | | | | | | | | | | | |
|---------------|--------------------------------|------|-----------------------------|----|-----|-----|--------------------------|-----------|-----------|--------------------------|-----------|
| BASE MATERIAL | | | Brick number 1 | | | | Brick number 2 | | | Brick number 3 | |
| ANCHOR TYPE | | | Installation without sleeve | | | | Installation with sleeve | | | Installation with sleeve | |
| DIMENSION | | | M6 | M8 | M10 | M12 | M8 | M10 | M12 | M6 | M8 |
| l_s | Plastic sleeve length | [mm] | - | - | - | - | 85 | 85 | 85 | 80 | 80 |
| d_o | Nominal diameter | [mm] | - | - | - | - | 16 | 16 | 16 | 12 | 12 |
| v | Mortar volume per sleeve | [ml] | - | - | - | - | - | - | - | - | - |
| d_o | Drill bit diameter | [mm] | 8 | 10 | 12 | 14 | 16 | 16 | 16 | 12 | 12 |
| h_1 | Drill hole depth \geq | [mm] | 80 | 90 | 90 | 90 | 90 | 90 | 90 | 85 | 85 |
| h_{ef} | Stud depth \geq | [mm] | 80 | 90 | 90 | 90 | 85 | 85 | 85 | 80 | 80 |
| h_{nom} | Sleeve installation depth | [mm] | - | - | - | - | 85 | 85 | 85 | 80 | 80 |
| d_f | Diameter in metal sheet \leq | [mm] | 7 | 9 | 12 | 14 | 9 | 12 | 14 | 9 | 9 |
| T_{ins} | Tightening torque \leq | [Nm] | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| d_b | Circular brush | [mm] | 9 | 14 | 14 | 14 | 20 | 20 | 20 | 14 | 14 |
| | Sleeve code | | . | . | . | . | MOTN15085 | MOTN15085 | MOTN20080 | MOTN12080 | MOTN12080 |

| | | M6 | | | M8 | | | M10/M12 | | |
|-------------------------------------|------|--------------------|------------------------|------------------------------|--------------------|------------------------|------------------------------|--------------------|------------------------|------------------------------|
| Minimum distances and from the edge | | $C_{cr} = C_{min}$ | $S_{cr } = S_{min }$ | $S_{cr\perp} = S_{min\perp}$ | $C_{cr} = C_{min}$ | $S_{cr } = S_{min }$ | $S_{cr\perp} = S_{min\perp}$ | $C_{cr} = C_{min}$ | $S_{cr } = S_{min }$ | $S_{cr\perp} = S_{min\perp}$ |
| Brick number 1 | [mm] | 120 | 240 | 240 | 135 | 270 | 270 | 135 | 270 | 270 |
| Brick number 2 | [mm] | - | - | - | 100 | 373 | 238 | 100 | 373 | 238 |
| Brick number 3 | [mm] | 100 | 245 | 110 | 100 | 245 | 110 | - | - | - |





MO-VSF

| INSTALLATION ACCESSORIES | | | INSTALLATION PROCEDURE |
|--------------------------|------------------|---|------------------------|
| CODE | PRODUCT | MATERIAL | BRICK |
| MOPISSI | APPLICATION GUNS | Gun for 300 ml cartridges | |
| MOPISTO | | Guns for 410 ml cartridges, professional use | |
| MOPISNEU | | Pneumatic gun for 410 ml coaxial cartridges, professional use | |
| MO-ES | STUD | Threaded stud | |
| MORCEPKIT | CLEANING BRUSHES | Kit with 3 cleaning brushes measuring $\varnothing 14$, $\varnothing 20$ and $\varnothing 29$ mm | |
| MOBOMBA | CLEANING PUMP | Pump for cleaning leftover dust and fragments in the drill hole | |
| MORCANU | MIXING TUBE | Plastic. Static labyrinth mixture | |
| MO-TN | NYLON SLEEVE | Plastic white or grey | |
| MO-TM | METAL SLEEVE | Metal sleeve $\varnothing 12$, $\varnothing 16$ and $\varnothing 22$ mm | |

| MINIMUM CURING TIME | | | | |
|---------------------|----------------------------|---------------------|--------------------------------|-------------------|
| TYPE | Cartridge temperature [°C] | Handling time [min] | Base material temperature [°C] | Curing time [min] |
| MO-VSF | min +5 | 18 | min +5 | 145 |
| | +5 a +10 | 10 | +5 a +10 | 145 |
| | +10 a +20 | 6 | +10 a +20 | 85 |
| | +20 a +25 | 5 | +20 a +25 | 50 |
| | +25 a +30 | 4 | +25 a +30 | 40 |
| | +30 | 4 | +30 | 35 |



MO-VSF

Characteristic resistances (F_{Rk})

| Anchor type | | Threaded studs. Tensile and shear force [kN] | | | | | | | |
|----------------|----------|--|-----|-----|-----|-----|-----|-----|-----|
| Use conditions | | d/d, w/d | | | | w/w | | | |
| Base material | Sleeve | M6 | M8 | M10 | M12 | M6 | M8 | M10 | M12 |
| Brick number 1 | - | 1,5 | 1,5 | 1,5 | 1,5 | 1,5 | 1,5 | 1,5 | 1,5 |
| Brick number 2 | Ø16 x 85 | - | 1,5 | 1,5 | 1,5 | - | 1,5 | 1,5 | 1,5 |
| Brick number 3 | Ø12 x 80 | 1,2 | 1,2 | - | - | 0,9 | 0,9 | - | - |

Calculated resistances (F_{Rd})

| Anchor type | | Threaded studs. Tensile and shear force [kN] | | | | | | | |
|----------------|----------|--|------|-----|-----|------|------|-----|-----|
| Use conditions | | d/d, w/d | | | | w/w | | | |
| Base material | Sleeve | M6 | M8 | M10 | M12 | M6 | M8 | M10 | M12 |
| Brick number 1 | - | 0,6 | 0,6 | 0,6 | 0,6 | 0,6 | 0,6 | 0,6 | 0,6 |
| Brick number 2 | Ø16 x 85 | - | 0,6 | 0,6 | 0,6 | - | 0,6 | 0,6 | 0,6 |
| Brick number 3 | Ø12 x 80 | 0,48 | 0,48 | - | - | 0,36 | 0,36 | - | - |

Recommended maximum loads (F_{recom}) (con $\gamma F= 1,4$)

| Use conditions | | d/d, w/d | | | | w/w | | | |
|----------------|----------|----------|------|------|------|------|------|------|------|
| Base material | Sleeve | M6 | M8 | M10 | M12 | M6 | M8 | M10 | M12 |
| Brick number 1 | - | 0,43 | 0,43 | 0,43 | 0,43 | 0,43 | 0,43 | 0,43 | 0,43 |
| Brick number 2 | Ø16 x 85 | - | 0,43 | 0,43 | 0,43 | - | 0,43 | 0,43 | 0,43 |
| Brick number 3 | Ø12 x 80 | 0,34 | 0,34 | - | - | 0,26 | 0,26 | - | - |

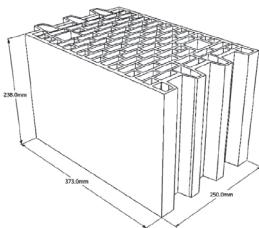


MO-VSF

BRICK TYPES

**Brick no. 1**

Solid clay brick Mz 12-2,0-NF according to EN 771-1
Length / width / height: 240 mm / 116 mm / 71 mm
 $f_b \geq 12 \text{ N/mm}^2$ / $\rho \geq 2,0 \text{ kg/dm}^3$

**Brick no. 2**

Hollow clay brick Porotherm 25 P+W KL15 according to EN 771-1
Length / width / height: 373 mm / 250 mm / 238 mm
 $f_b \geq 12 \text{ N/mm}^2$ / $\rho \geq 0,9 \text{ kg/dm}^3$

**Brick no. 3**

Perforated clay brick 10 according to EN 771-1
Length / width / height: 245 mm / 110 mm / 100 mm
 $f_b \geq 15 \text{ N/mm}^2$ / $\rho \geq 2,05 \text{ kg/dm}^3$



MO-VSF

RETROFITTED REBAR CONNECTIONS

This technical document covers post-installed rebar connections in non-carbonate concrete under the assumption that post-installed rebar connections are generally calculated according to Eurocode 2. The rebar anchor system comprises the bonding of the material and a straight, recessed reinforcement rebar with the properties specified in Eurocode 2, Annex C; classes B and C.

Dynamic, fatigue or seismic loads on post-installed rebar connections are not covered by this technical document.

Intended use

This technical document covers application in non-carbonate concrete only from C12/15 to C50/60 [EN 206] for the following applications:

- Overlapping bond with an existing rebar in a building component (Figures 1 and 4).
- Fixing of rebar in a slab or in a support. Support at one end of a slab calculated as simply supported as well as its rebars for retention forces (Figure 2).
- Fixing of rebar of construction components mainly subjected to compression (Figure 3).
- Fixing of rebar to cover the action line of the tensile force (Figure 5).

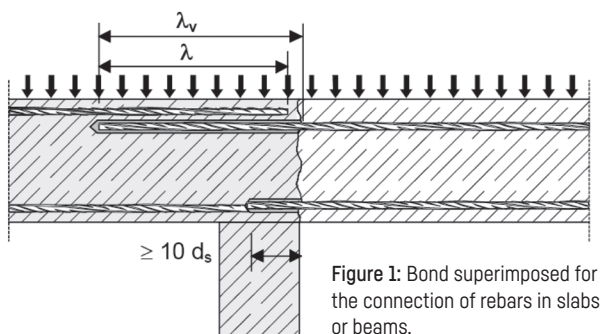


Figure 1: Bond superimposed for the connection of rebars in slabs or beams.

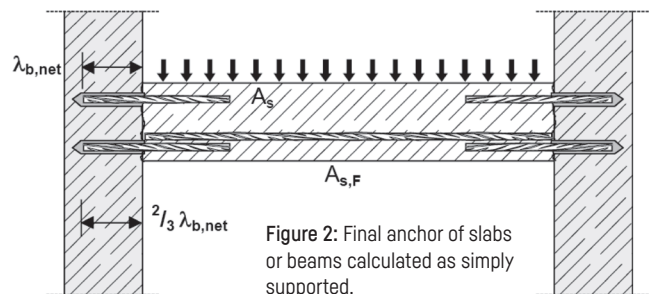


Figure 2: Final anchor of slabs or beams calculated as simply supported.

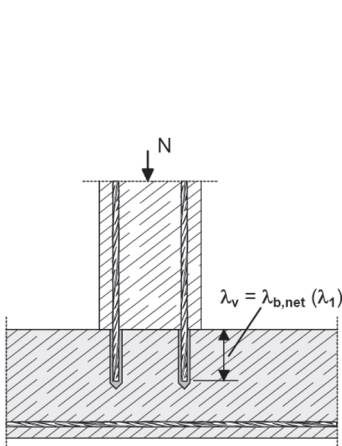


Figure 3: Rebar connections for items primarily subjected to compression. The rebars are subjected to compression.

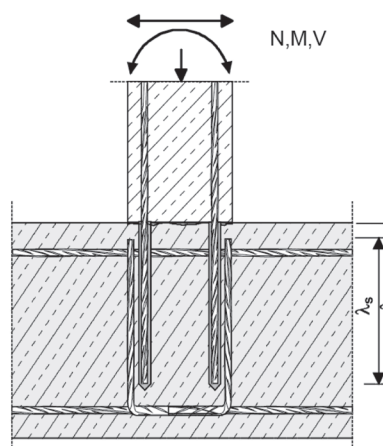


Figure 4: Bond superimposed to a foundation of a column or a wall where the rebars is subjected to tensile force.

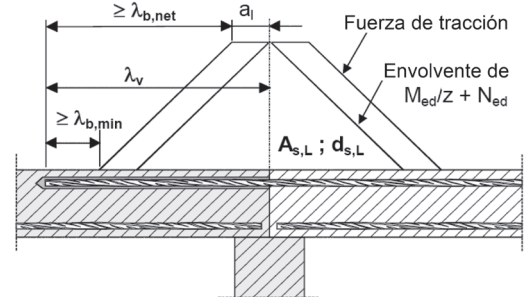


Figure 5: Reinforcement anchor to cover the action line of the tensile force.

* Note for Figure 1 and 5: In the figures the transversal reinforcements have not been represented, the transversal reinforcements as required by the Eurocode 2 must be present. The shear stress transferred between the anterior and posterior concrete must be calculated according to Eurocode 2.



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The tables shown below refer to Eurocode 2 Annex C, Table C.1 and C2N, rebar properties.

| Properties of the start rebars | | | | |
|--|---|-------------------------|-------------|--|
| Product form | | Rebars and unwound rods | | |
| Class | | B | C | |
| Characteristic yield stress f_{yk} or $f_{0.2k}$ (MPa) | | 400 to 600 | | |
| Minimum value of $k = (f_t / f_{yk})_k$ | | ≥ 1.08 | ≥ 1.15 | |
| Characteristic maximum tensile deformation ϵ_{uk} (%) | | ≥ 5.0 | ≥ 7.5 | |
| Flexibility | | Bending/folding test | | |
| Maximum deviation from the nominal weight (individual bar or wire) (%) | Nominal size of the rebar (mm) $\leq 8 > 8$ | ± 6.0 | | |
| | | ± 4.5 | | |
| Bonding: | Nominal size of the rebar (mm) 8 to 12 > 12 | 0.040 | | |
| Minimum relative corrugated area, $f_{R,min}$ | | 0.056 | | |

| Minimum / maximum lengths* | | | | |
|----------------------------|--------------------------------|-------------------------|---------------------|-----------|
| Rebar | Minimum | | | Maximum |
| $\varnothing d_s$ [mm] | $f_{y,k}$ [N/mm ²] | Anchor $l_{b,min}$ [mm] | Overlap $l_{o,min}$ | l_{max} |
| 8 | 500 | 114 | 200 | 400 |
| 10 | 500 | 142 | 200 | 500 |
| 12 | 500 | 171 | 200 | 600 |
| 14 | 500 | 199 | 210 | 700 |
| 16 | 500 | 227 | 240 | 800 |

*For concrete C20/25 ($f_{bd} = 2,3$ N/mm²), good bond conditions, rebar ($f_{yk} = 500$ N/mm²)

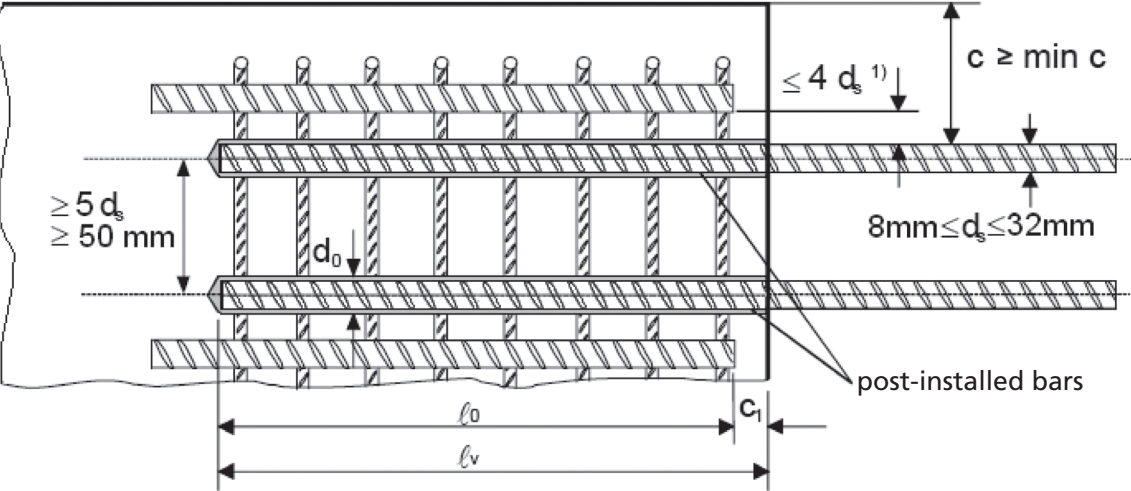
| Design bond resistance | | | | | | | | | | |
|------------------------|-----------------------|----------------------|--------|--------|--------|--------|------------------|--------|--------|--------|
| Rebar \varnothing | Resistance and factor | Concrete class | | | | | | | | |
| d_s [mm] | | C12/15 | C16/20 | C20/25 | C25/30 | C30/37 | C35/45 | C40/50 | C45/55 | C50/60 |
| 8 | k_b^* | 1 | 1 | 1 | 0,86 | 0,76 | 0,69 | 0,63 | 0,58 | 0,54 |
| | $f_{bd,PIR}$ | 1,6 | 2 | 2,3 | | | | | | |
| 10 a 16 | k_b^* | 1 | 1 | 1 | 1 | 0,89 | 0,8 | 0,73 | 0,67 | 0,63 |
| | $f_{bd,PIR}$ | 1,6 | 2 | 2,3 | 2,7 | | | | | |
| Bar \varnothing | | Amplification factor | | | | | Concrete class | | | |
| d_s [mm] | | | | | | | C12/15 to C50/60 | | | |
| 8 a 16 | | α_{ib} | | | | | 1,5 | | | |

*For all drilling methods with good bond conditions

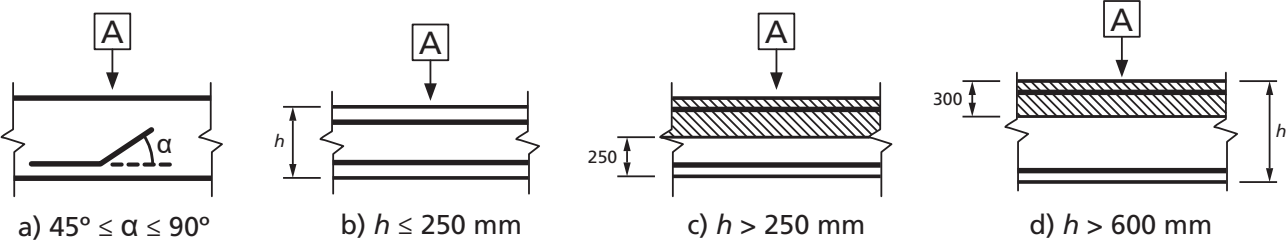


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- Calculated load values according to Eurocode 2 and EOTA technical report TR 023.
- Information according to ETA 13/0780.
- Non-cracked concrete, conditions in dry or wet conditions.
- Temperature range: -40°C to +80°C [maximum long-term temperature +50°C].
- Minimum spacing conditions between bars $\geq 5d_s$, min. 50 mm:



- Minimum concrete coating:
 - drilling with compressed air $\geq 50 + 0.06 L_b$
 - drilling in percussion mode $\geq 30 + 0.08 L_b \geq 2\Phi$
- Good bonding conditions:



A Direction of the concreting (a) and (b) "good" bonding conditions for all types of bars. (c) and (d) without shaded area - "good" bonding conditions. Shaded area- "poor" bonding conditions.

* In case of poor bonding conditions, multiply values by 0.7.



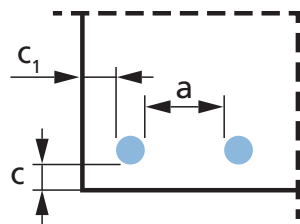
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Resistance values may increase in the following situations:

- With transverse tension/compression pressure (α_2)
- In case of concrete coating (α_5)
- In case of overlapping rebars (α_6)

| Values for α_2 , α_5 and α_6 | | |
|---|--|------------------|
| Influence factor | Reinforcement bar | |
| | A tension | A compression |
| Concrete coating | $\alpha_2 = 1 - 0.15 (cd - \emptyset) / \emptyset$ ≥ 0.7 ≤ 1.0 | $\alpha_2 = 1.0$ |
| Transverse pressure confinement | $\alpha_5 = 1 - 0.004p$ ≥ 0.7 ≤ 1.0 | $\alpha_5 = 1.0$ |
| Overlapping length | $\alpha_6 = (p_1 / 25)^{0.25}$ ≥ 1.0 ≤ 1.5 | |

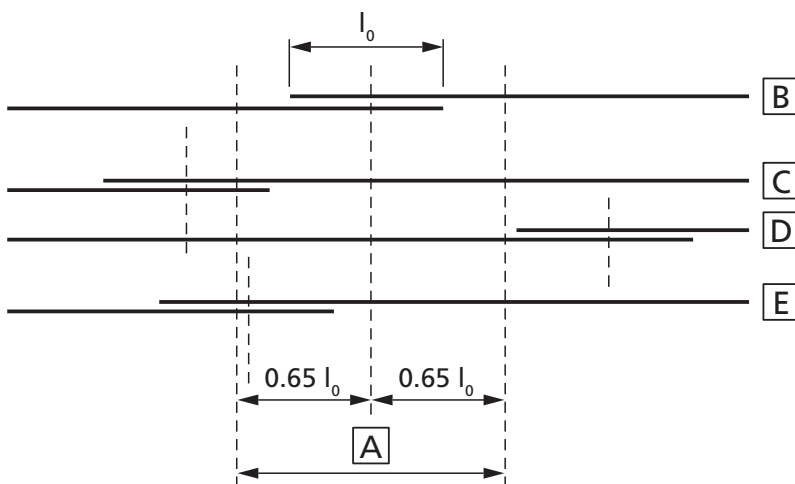
Where:



$c_d = \min (a/2, c_1, c)$

p : transverse pressure [MPa] in the ultimate limit state I_{bd}

p_1 is the percentage of the overlapped reinforcement bar within $0.65 \cdot l_0$ from the centre of the length of the overlap considered



- A** Section considered
- B** Bar I
- C** Bar II
- D** Bar III
- E** Bar IV



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TABLES OF PRECALCULATED VALUES

| Concrete class 20/25 | | | | | | | | |
|---|-----------------|----------------------|---|--------|--------|------------------|--------|--|
| Concrete compressive strength [$f_{ck,cube}$]: 25 N/mm ² | | | | | | | | |
| Rebar Ø | d_s | [mm] | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | |
| Rebar Size | d_s | [mm] | 8 | 10 | 12 | 14 | 16 | |
| Cross-sectional area | A_s | [mm ²] | 50,3 | 78,5 | 113,1 | 153,9 | 201,1 | |
| Characteristic yield strength of rebar | f_{yk} | [N/mm ²] | 500 | 500 | 500 | 500 | 500 | |
| Partial safety factor | $\gamma_{M,s}$ | [-] | 1,15 | 1,15 | 1,15 | 1,15 | 1,15 | |
| Design yield strength of rebar | f_{yd} | [N/mm ²] | 434,78 | 434,78 | 434,78 | 434,78 | 434,78 | |
| Design steel resistance | $N_{Rd,s}$ | [kN] | 21,9 | 34,1 | 49,2 | 66,9 | 87,4 | |
| Bond stress | f_{bd} | [N/mm ²] | 2,3 | 2,3 | 2,3 | 2,3 | 2,3 | |
| Amplification factor for minimum anchorage length | α_{lb} | [-] | 1 | 1 | 1 | 1 | 1 | |
| Basic Anchorage Length - Applied | $l_{b,rqd}$ | [mm] | 0 | 0 | 0 | 0 | 0 | |
| Basic Anchorage Length - Yield | $l_{b,rqd,yld}$ | [mm] | 378,07 | 472,59 | 567,11 | 661,63 | 756,14 | |
| Minimum anchorage Length | $l_{b,min}$ | [mm] | 113,42 | 141,78 | 170,13 | 198,49 | 226,84 | |
| Minimum lap length | $l_{0,min}$ | [mm] | 200 | 200 | 200 | 210 | 240 | |
| Max permissible embedment depth | $l_{v,max}$ | [mm] | 400 | 500 | 600 | 700 | 800 | |
| Drilled hole diameter | d_h | [mm] | 12 | 14 | 16 | 18 | 20 | |
| Bar spacing \geq | s | [mm] | 50 | 50 | 60 | 70 | 80 | |
| Edge distance (compressed air drilling) \geq | c | [mm] | 50 + 0,06 L_b | | | | | |
| Edge distance (hammer drilling) \geq | c | [mm] | 30 + 0,08 $L_b \geq 2\Phi$ | | | | | |
| Anchorage Length, L_b [mm] | | | Design tensile pull-out bond resistance, N_{Rd} | | | | | |
| 114 | 6,6 | | | | | | | |
| 142 | 8,2 | 10,3 | | | | Not allowed area | | |
| 171 | 9,9 | 12,4 | 14,8 | | | | | |
| 199 | 11,5 | 14,4 | 17,3 | 20,1 | | | | |
| 200 | 11,6 | 14,5 | 17,3 | 20,2 | | | | |
| 210 | 12,1 | 15,2 | 18,2 | 21,2 | | | | |
| 227 | 13,1 | 16,4 | 19,7 | 23 | 26,2 | | | |
| 240 | 13,9 | 17,3 | 20,8 | 24,3 | 27,7 | | | |
| 300 | 17,3 | 21,7 | 26 | 30,3 | 34,7 | | | |
| 350 | 20,2 | 25,3 | 30,3 | 35,4 | 40,5 | | | |
| 400 | 21,9 | 28,9 | 34,7 | 40,5 | 46,2 | | | |
| 450 | | 32,5 | 39 | 45,5 | 52 | | | |
| 500 | | 34,1 | 43,4 | 50,6 | 57,8 | | | |
| 550 | | | 47,7 | 55,6 | 63,6 | | | |
| 600 | | | 49,2 | 60,7 | 69,4 | | | |
| 650 | | | | 65,8 | 75,1 | | | |
| 700 | | | | 66,9 | 80,9 | | | |
| 750 | | | | | 86,7 | | | |
| 800 | | | | | 87,4 | | | |
| Length to develop steel yield, $L_{b,rqd}$ [mm] | 378 | 473 | 567 | 662 | 756 | | | |

Values shaded in blue are not allowed for overlapping joints



MO-VSF

TABLES OF PRECALCULATED VALUES

| Concrete class 30/37 | | | | | | | | |
|---|-----------------|----------------------|---|--------|--------|------------------|--------|--|
| Concrete compressive strength [$f_{ck,cube}$]: 37 N/mm ² | | | | | | | | |
| Rebar Ø | d_s | [mm] | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | |
| Rebar Size | d_s | [mm] | 8 | 10 | 12 | 14 | 16 | |
| Cross-sectional area | A_s | [mm ²] | 50,3 | 78,5 | 113,1 | 153,9 | 201,1 | |
| Characteristic yield strength of rebar | f_{yk} | [N/mm ²] | 500 | 500 | 500 | 500 | 500 | |
| Partial safety factor | $\gamma_{M,s}$ | [-] | 1,15 | 1,15 | 1,15 | 1,15 | 1,15 | |
| Design yield strength of rebar | f_{yd} | [N/mm ²] | 434,78 | 434,78 | 434,78 | 434,78 | 434,78 | |
| Design steel resistance | $N_{Rd,s}$ | [kN] | 21,9 | 34,1 | 49,2 | 66,9 | 87,4 | |
| Bond stress | f_{bd} | [N/mm ²] | 2,3 | 3 | 3 | 3 | 3 | |
| Amplification factor for minimum anchorage length | α_{lb} | [-] | 0,76 | 0,89 | 0,89 | 0,89 | 0,89 | |
| Basic Anchorage Length - Applied | $l_{b,rqd}$ | [mm] | 0 | 0 | 0 | 0 | 0 | |
| Basic Anchorage Length - Yield | $l_{b,rqd,yld}$ | [mm] | 378,07 | 362,32 | 434,78 | 507,25 | 579,71 | |
| Minimum anchorage Length | $l_{b,min}$ | [mm] | 86,2 | 96,74 | 116,09 | 135,43 | 154,78 | |
| Minimum lap length | $l_{0,min}$ | [mm] | 152 | 178 | 178 | 186,9 | 213,6 | |
| Max permissible embedment depth | $l_{v,max}$ | [mm] | 400 | 500 | 600 | 700 | 800 | |
| Drilled hole diameter | d_h | [mm] | 12 | 14 | 16 | 18 | 20 | |
| Bar spacing \geq | s | [mm] | 50 | 50 | 60 | 70 | 80 | |
| Edge distance (compressed air drilling) \geq | c | [mm] | 50 + 0,06 L_b | | | | | |
| Edge distance (hammer drilling) \geq | c | [mm] | 30 + 0,08 $L_b \geq 2\Phi$ | | | | | |
| Anchorage Length, L_b [mm] | | | Design tensile pull-out bond resistance, N_{Rd} | | | | | |
| 87 | 5 | | | | | | | |
| 97 | 5,6 | 9,1 | | | | Not allowed area | | |
| 117 | 6,8 | 11 | 13,2 | | | | | |
| 136 | 7,9 | 12,8 | 15,4 | 17,9 | | | | |
| 152 | 8,8 | 14,3 | 17,2 | 20,1 | | | | |
| 155 | 9 | 14,6 | 17,5 | 20,5 | 23,4 | | | |
| 178 | 10,3 | 16,8 | 20,1 | 23,5 | 26,8 | | | |
| 187 | 10,8 | 17,6 | 21,1 | 24,7 | 28,2 | | | |
| 214 | 12,4 | 20,2 | 24,2 | 28,2 | 32,3 | | | |
| 250 | 14,5 | 23,6 | 28,3 | 33 | 37,7 | | | |
| 300 | 17,3 | 28,3 | 33,9 | 39,6 | 45,2 | | | |
| 350 | 20,2 | 33 | 39,6 | 46,2 | 52,8 | | | |
| 400 | 21,9 | 34,1 | 45,2 | 52,8 | 60,3 | | | |
| 450 | | 34,1 | 49,2 | 59,4 | 67,9 | | | |
| 500 | | 34,1 | 49,2 | 66 | 75,4 | | | |
| 550 | | | 49,2 | 66,9 | 82,9 | | | |
| 600 | | | 49,2 | 66,9 | 87,4 | | | |
| 650 | | | | 66,9 | 87,4 | | | |
| 700 | | | | 66,9 | 87,4 | | | |
| 750 | | | | | 87,4 | | | |
| 800 | | | | | 87,4 | | | |
| Length to develop steel yield, $L_{b,rqd}$ [mm] | 378 | 362 | 435 | 507 | 580 | | | |

Values shaded in blue are not allowed for overlapping joints



MO-VSF

TABLES OF PRECALCULATED VALUES

| Concrete class 40/50 | | | | | | | | | |
|---|-----------------|----------------------|---|--------|--------|--------|--------|------|------|
| Concrete compressive strength [$f_{ck,cube}$]: 50 N/mm ² | | | | | | | | | |
| Rebar Ø | d_s | [mm] | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | | |
| Rebar Size | d_s | [mm] | 8 | 10 | 12 | 14 | 16 | | |
| Cross-sectional area | A_s | [mm ²] | 50,3 | 78,5 | 113,1 | 153,9 | 201,1 | | |
| Characteristic yield strength of rebar | f_{yk} | [N/mm ²] | 500 | 500 | 500 | 500 | 500 | | |
| Partial safety factor | $\gamma_{M,s}$ | [-] | 1,15 | 1,15 | 1,15 | 1,15 | 1,15 | | |
| Design yield strength of rebar | f_{yd} | [N/mm ²] | 434,78 | 434,78 | 434,78 | 434,78 | 434,78 | | |
| Design steel resistance | $N_{Rd,s}$ | [kN] | 21,9 | 34,1 | 49,2 | 66,9 | 87,4 | | |
| Bond stress | f_{bd} | [N/mm ²] | 2,3 | 3,7 | 3,7 | 3,7 | 3,7 | | |
| Amplification factor for minimum anchorage length | α_{lb} | [-] | 0,63 | 0,73 | 0,73 | 0,73 | 0,73 | | |
| Basic Anchorage Length - Applied | $l_{b,rqd}$ | [mm] | 0 | 0 | 0 | 0 | 0 | | |
| Basic Anchorage Length - Yield | $l_{b,rqd,fyd}$ | [mm] | 378,07 | 293,77 | 352,53 | 411,28 | 470,04 | | |
| Minimum anchorage Length | $l_{b,min}$ | [mm] | 71,46 | 73 | 87,6 | 102,2 | 116,8 | | |
| Minimum lap length | $l_{0,min}$ | [mm] | 126 | 146 | 146 | 153,3 | 175,2 | | |
| Max permissible embedment depth | $l_{v,max}$ | [mm] | 400 | 500 | 600 | 700 | 800 | | |
| Drilled hole diameter | d_h | [mm] | 12 | 14 | 16 | 18 | 20 | | |
| Bar spacing \geq | s | [mm] | 50 | 50 | 60 | 70 | 80 | | |
| Edge distance (compressed air drilling) \geq | c | [mm] | 50 + 0,06 L_b | | | | | | |
| Edge distance (hammer drilling) \geq | c | [mm] | 30 + 0,08 $L_b \geq 2\Phi$ | | | | | | |
| Anchorage Length, L_b [mm] | | | Design tensile pull-out bond resistance, N_{Rd} | | | | | | |
| 72 | 4,2 | | Not allowed area | | | | | | |
| 73 | 4,2 | 8,5 | | | | | | | |
| 88 | 5,1 | 10,2 | | | | | 12,3 | | |
| 103 | 6 | 12 | | | | | 14,4 | 16,8 | |
| 117 | 6,8 | 13,6 | | | | | 16,3 | 19 | 21,8 |
| 126 | 7,3 | 14,6 | | | | | 17,6 | 20,5 | 23,4 |
| 146 | 8,4 | 17 | | | | | 20,4 | 23,8 | 27,2 |
| 154 | 8,9 | 17,9 | | | | | 21,5 | 25,1 | 28,6 |
| 176 | 10,2 | 20,5 | | | | | 24,5 | 28,6 | 32,7 |
| 400 | 21,9 | 34,1 | | | | | 49,2 | 65,1 | 74,4 |
| 450 | | 34,1 | 49,2 | 66,9 | 83,7 | | | | |
| 500 | | 34,1 | 49,2 | 66,9 | 87,4 | | | | |
| 550 | | | 49,2 | 66,9 | 87,4 | | | | |
| 600 | | | 49,2 | 66,9 | 87,4 | | | | |
| 650 | | | | 66,9 | 87,4 | | | | |
| 700 | | | | 66,9 | 87,4 | | | | |
| 750 | | | | | 87,4 | | | | |
| 800 | | | | | 87,4 | | | | |
| Length to develop steel yield, $L_{b,rqd}$ [mm] | | | 378 | 294 | 353 | 411 | 470 | | |

Values shaded in blue are not allowed for overlapping joints



MO-VSF

TABLES OF PRECALCULATED VALUES

| Concrete class 50/60 | | | | | | | | |
|---|-----------------|----------------------|---|--------|--------|------------------|--------|--|
| Concrete compressive strength [$f_{ck,cube}$]: 60 N/mm ² | | | | | | | | |
| Rebar Ø | d_s | [mm] | Ø8 | Ø10 | Ø12 | Ø14 | Ø16 | |
| Rebar Size | d_s | [mm] | 8 | 10 | 12 | 14 | 16 | |
| Cross-sectional area | A_s | [mm ²] | 50,3 | 78,5 | 113,1 | 153,9 | 201,1 | |
| Characteristic yield strength of rebar | f_{yk} | [N/mm ²] | 500 | 500 | 500 | 500 | 500 | |
| Partial safety factor | $\gamma_{M,s}$ | [-] | 1,15 | 1,15 | 1,15 | 1,15 | 1,15 | |
| Design yield strength of rebar | f_{yd} | [N/mm ²] | 434,78 | 434,78 | 434,78 | 434,78 | 434,78 | |
| Design steel resistance | $N_{Rd,s}$ | [kN] | 21,9 | 34,1 | 49,2 | 66,9 | 87,4 | |
| Bond stress | f_{bd} | [N/mm ²] | 2,3 | 4,3 | 4,3 | 4,3 | 4,3 | |
| Amplification factor for minimum anchorage length | α_{lb} | [-] | 0,54 | 0,63 | 0,63 | 0,63 | 0,63 | |
| Basic Anchorage Length - Applied | $l_{b,rqd}$ | [mm] | 0 | 0 | 0 | 0 | 0 | |
| Basic Anchorage Length - Yield | $l_{b,rqd,fyd}$ | [mm] | 378,07 | 252,78 | 303,34 | 353,89 | 404,45 | |
| Minimum anchorage Length | $l_{b,min}$ | [mm] | 61,25 | 63 | 75,6 | 88,2 | 100,8 | |
| Minimum lap length | $l_{0,min}$ | [mm] | 108 | 126 | 126 | 132,3 | 151,2 | |
| Max permissible embedment depth | $l_{v,max}$ | [mm] | 400 | 500 | 600 | 700 | 800 | |
| Drilled hole diameter | d_h | [mm] | 12 | 14 | 16 | 18 | 20 | |
| Bar spacing \geq | s | [mm] | 50 | 50 | 60 | 70 | 80 | |
| Edge distance (compressed air drilling) \geq | c | [mm] | 50 + 0,06 L_b | | | | | |
| Edge distance (hammer drilling) \geq | c | [mm] | 30 + 0,08 $L_b \geq 2\Phi$ | | | | | |
| Anchorage Length, L_b [mm] | | | Design tensile pull-out bond resistance, N_{Rd} | | | | | |
| 62 | 3,6 | | | | | | | |
| 63 | 3,6 | 8,5 | | | | Not allowed area | | |
| 76 | 4,4 | 10,3 | 12,3 | | | | | |
| 89 | 5,1 | 12 | 14,4 | 16,8 | | | | |
| 101 | 5,8 | 13,6 | 16,4 | 19,1 | 21,8 | | | |
| 108 | 6,2 | 14,6 | 17,5 | 20,4 | 23,3 | | | |
| 126 | 7,3 | 17 | 20,4 | 23,8 | 27,2 | | | |
| 133 | 7,7 | 18 | 21,6 | 25,2 | 28,7 | | | |
| 152 | 8,8 | 20,5 | 24,6 | 28,7 | 32,9 | | | |
| 400 | 21,9 | 34,1 | 49,2 | 66,9 | 86,5 | | | |
| 450 | | 34,1 | 49,2 | 66,9 | 87,4 | | | |
| 500 | | 34,1 | 49,2 | 66,9 | 87,4 | | | |
| 550 | | | 49,2 | 66,9 | 87,4 | | | |
| 600 | | | 49,2 | 66,9 | 87,4 | | | |
| 650 | | | | 66,9 | 87,4 | | | |
| 700 | | | | 66,9 | 87,4 | | | |
| 750 | | | | | 87,4 | | | |
| 800 | | | | | 87,4 | | | |
| Length to develop steel yield, $L_{b,rqd}$ [mm] | 378 | 253 | 303 | 354 | 404 | | | |

Values shaded in blue are not allowed for overlapping joints



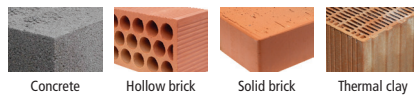
MO-VSF

RANGE

VINYL ESTER STYRENE-FREE



| CODE | DIMENSION | |
|---------------|-----------|----|
| NORMAL | | |
| MOVSF300 | 300 ml | 12 |
| MOVSF410 | 410 ml | 12 |



Accessories for chemical anchor cartridges

MO-PIS Application guns



| CODE | MODEL |
|----------|---------------------|
| MOPISTO | Manual |
| MOPISPR | Professional 410 ml |
| MOPISSI | Silicone 300 ml |
| MOPISNEU | Pneumatic |

MO-TN Plastic sleeve



| CODE | DIMENSION |
|-----------|-----------|
| MOTN12050 | 12 x 50 |
| MOTN12080 | 12 x 80 |
| MOTN15085 | 15 x 85 |
| MOTN15130 | 15 x 130 |
| MOTN20085 | 20 x 85 |

MO-AC Mixing tubes and miscellaneous



| CODE | MODEL |
|-----------|-------------------|
| MOBOMBA | Blower pump |
| MORCANU | Tube 300 - 410 ml |
| MORCEPKIT | Kit 3 brushes |

MO-ES Threaded stud



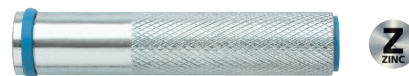
| CODE | DIMENSION |
|-----------|-----------|
| MOES06070 | M6 x 70 |
| MOES08110 | M8 x 110 |
| MOES10115 | M10 x 115 |
| MOES12110 | M12 x 110 |

MO-TM Metal sleeve



| CODE | DIMENSION |
|-----------|-----------|
| MOTM12100 | 12 x 1000 |
| MOTM16100 | 16 x 1000 |
| MOTM22100 | 22 x 1000 |

MO-TR Threaded sleeve



| CODE | DIMENSION |
|---------|-------------|
| MOTRO08 | M8/12 x 80 |
| MOTRO10 | M10/14 x 80 |
| MOTRO12 | M12/16 x 80 |



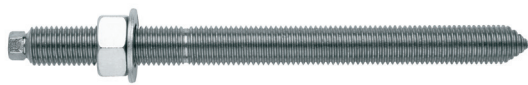
MO-VSF

Accessories for chemical anchor cartridges

Stud for chemical anchor with nut and washer

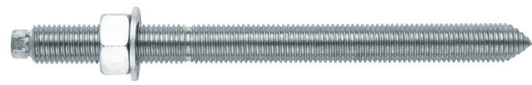


EQ-AC Zinc-plated 5.8



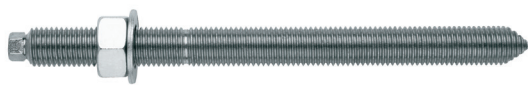
| CODE | DIMENSION |
|-----------|-----------|
| EQAC08110 | M8 x 110 |
| EQAC10130 | M10 x 130 |
| EQAC10190 | M10 x 190 |
| EQAC12160 | M12 x 160 |
| EQAC12220 | M12 x 220 |
| EQAC16190 | M16 x 190 |
| EQAC16250 | M16 x 250 |
| EQAC20260 | M20 x 260 |
| EQAC20350 | M20 x 350 |
| EQAC24300 | M24 x 300 |
| EQAC24380 | M24 x 380 |
| EQAC30330 | M30 x 330 |

EQ-A2 Stainless steel A2



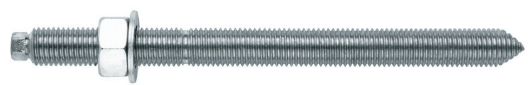
| CODE | DIMENSION |
|-----------|-----------|
| EQA208110 | M8 x 110 |
| EQA210130 | M10 x 130 |
| EQA212160 | M12 x 160 |
| EQA216190 | M16 x 190 |
| EQA220260 | M20 x 260 |
| EQA224300 | M24 x 300 |
| EQA230330 | M30 x 330 |

EQ-8.8 Zinc-plated 8.8



| CODE | DIMENSION |
|-----------|-------------|
| EQ8808110 | M8 x 110/40 |
| EQ8810130 | M10 x 130 |
| EQ8812160 | M12 x 160 |
| EQ8816190 | M16 x 190 |
| EQ8820260 | M20 x 260 |
| EQ8824300 | M24 x 300 |

EQ-A4 Stainless steel A4



| CODE | DIMENSION |
|-----------|-----------|
| EQA408110 | M8 x 110 |
| EQA410130 | M10 x 130 |
| EQA412160 | M12 x 160 |
| EQA416190 | M16 x 190 |
| EQA420260 | M20 x 260 |
| EQA424300 | M24 x 300 |
| EQA430330 | M30 x 330 |

