## TDE / TLE

## Reference: FT TDE-en





## CHARACTERISTICS

- Pilot hole in concrete needed; thread is created by the anchor during the installation process
- No special drill bit required; install using standard-sized ANSI tolerance drill bits
- Code listed under IBC/IRC in accordance with ICC-ES AC193 and ACl 355.2 for cracked and uncracked concrete and AC01 for masonry elements.
- Qualified for static, wind and seismic loading conditions
- Removable, leaving concrete surface flat. Ideal for temporary anchoring (e.g. formwork, bracing) or applications where fixtures may need to be moved
- Suitable when reduced edge distances or spacing required
- Atlantis (TDE) or zinc plated coating (TLE)


## APPROVALS



ESR-4314
ESR-5216

Florida approval FL30477
Codes compliance: IBC/IRC 2021, 2018, 2015 ,

2013, 2009
LABC/LARC 2023
CBC/CRC 2022
FBC 2023


1. RANGE

| ITEM | COED | SIZE | PICTURE | COMPONENT | MATERIAL |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | TDE | $1 / 4 "-3 / 4 "$ | Hexagonal screw <br> anchor | Carbon steel, Atlantis coating |  |
| 2 | TLE | $1 / 4 "-3 / 4 "$ |  | Hexagonal screw <br> anchor | Carbon steel, zinc plated coating $\geq 0,0002$ in |

## TDE / TLE

## 2. INSTALLATION DETAILS IN CONCRETE



| Parameter | Symbol | Units | Nominal anchor diameter |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1/4" |  | 3/8" |  | 1/2" |  | 5/8" |  | 3/4" |  |
| Drill bit diameter | $\mathrm{d}_{0}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 1 / 4 \\ (6,4) \end{gathered}$ | $\begin{gathered} 1 / 4 \\ (6,4) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ |
| Nominal embedment depth ${ }^{1}$ | hnom | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 15 / 8 \\ & (41) \end{aligned}$ | $\begin{array}{r} 21 / 2 \\ (64) \end{array}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{aligned} & 41 / 4 \\ & (108) \end{aligned}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & 61 / 4 \\ & (159) \end{aligned}$ |
| Effective embedment depth | $h_{\text {ef }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 1,23 \\ & (31) \end{aligned}$ | $\begin{aligned} & 1,98 \\ & (50) \end{aligned}$ | $\begin{aligned} & 1.85 \\ & (47) \end{aligned}$ | $\begin{aligned} & 2.49 \\ & (63) \end{aligned}$ | $\begin{aligned} & 2.21 \\ & (56) \end{aligned}$ | $\begin{aligned} & 3.27 \\ & (83) \end{aligned}$ | $\begin{aligned} & 2.36 \\ & (60) \end{aligned}$ | $\begin{aligned} & 3.85 \\ & \text { (98) } \end{aligned}$ | $\begin{aligned} & 2.97 \\ & (75) \end{aligned}$ | $\begin{aligned} & 4.89 \\ & (124) \end{aligned}$ |
| Minimum hole depth | $h_{\text {hole }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 27 / 8 \\ (73) \end{gathered}$ | $\begin{gathered} 23 / 4 \\ (70) \end{gathered}$ | $\begin{aligned} & 31 / 2 \\ & (89) \end{aligned}$ | $\begin{gathered} 33 / 8 \\ (86) \end{gathered}$ | $\begin{aligned} & 45 / 8 \\ & (117) \end{aligned}$ | $\begin{aligned} & 35 / 8 \\ & (92) \end{aligned}$ | $\begin{aligned} & 53 / 8 \\ & (137) \end{aligned}$ | $\begin{aligned} & 43 / 8 \\ & (111) \end{aligned}$ | $\begin{aligned} & 65 / 8 \\ & (168) \end{aligned}$ |
| Maximum fixture clearance Hole diameter | $\mathrm{d}_{\mathrm{f}}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{gathered} 7 / 8 \\ (22.2) \end{gathered}$ | $\begin{gathered} 7 / 8 \\ (22.2) \end{gathered}$ |
| Maximum installation torque | $\mathrm{T}_{\text {inst.max }}$ | $\begin{gathered} \mathrm{ft} \mathrm{lb} \\ (\mathrm{Nm}) \end{gathered}$ | $\begin{gathered} 15 \\ (20) \end{gathered}$ | $\begin{gathered} 24 \\ (33) \end{gathered}$ | $\begin{gathered} 35 \\ (47) \end{gathered}$ | $\begin{gathered} 50 \\ (68) \end{gathered}$ | $\begin{gathered} 45 \\ (61) \end{gathered}$ | $\begin{gathered} 65 \\ (88) \end{gathered}$ | $\begin{gathered} 85 \\ (115) \end{gathered}$ | $\begin{gathered} 100 \\ (136) \end{gathered}$ | $\begin{gathered} 115 \\ (156) \end{gathered}$ | $\begin{gathered} 150 \\ (203) \end{gathered}$ |
| Maximum impact wrench torque rating | Timpact.max | $\begin{gathered} \mathrm{ft} \mathrm{lb} \\ (\mathrm{Nm}) \end{gathered}$ | $\begin{gathered} 150 \\ (203) \end{gathered}$ | $\begin{gathered} 150 \\ (203) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{aligned} & 380 \\ & (515) \end{aligned}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{aligned} & 380 \\ & (515) \end{aligned}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ |
| Minimum concrete thickness | $\mathrm{h}_{\text {min }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 31 / 4 \\ & (83) \end{aligned}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & 43 / 4 \\ & (121) \end{aligned}$ | $\begin{aligned} & 43 / 4 \\ & (121) \end{aligned}$ | $\begin{aligned} & 63 / 4 \\ & (171) \end{aligned}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{gathered} 7 \\ (178) \end{gathered}$ | $\begin{gathered} 6 \\ (152) \end{gathered}$ | $\begin{aligned} & 81 / 8 \\ & (206) \end{aligned}$ |
| Critical edge distance | Cac | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{aligned} & 33 / 4 \\ & (95) \end{aligned}$ | $\begin{gathered} 7 \\ (178) \end{gathered}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ |
| Minimum edge distance | $\mathrm{Cmin}^{\text {m }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 11 / 2 \\ & (38) \end{aligned}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{aligned} & 11 / 2 \\ & (38) \end{aligned}$ | $\begin{aligned} & 11 / 2 \\ & (38) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ |
| Minimum spacing | Smin | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ |
| Minimum overall anchor length ${ }^{2}$ | lanch | $\begin{gathered} \mathrm{in} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 13 / 4 \\ (44,5) \end{gathered}$ | $\begin{gathered} 25 / 8 \\ (66,7) \end{gathered}$ | $\begin{gathered} 23 / 4 \\ (70) \end{gathered}$ | $\begin{gathered} 31 / 2 \\ (89) \end{gathered}$ | $\begin{gathered} 31 / 4 \\ (82) \end{gathered}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{array}{r} 31 / 2 \\ (89) \end{array}$ | $\begin{aligned} & 51 / 4 \\ & (133) \end{aligned}$ | $\begin{aligned} & 41 / 4 \\ & (108) \end{aligned}$ | $\begin{aligned} & 61 / 2 \\ & (165) \end{aligned}$ |
| Spanner | Sw | in | 7/16 | 7/16 | 9/16 | 9/16 | 3/4 | 3/4 | 15/16 | 15/16 | $11 / 8$ | $11 / 8$ |
| Maximum fixture thickness | $\mathrm{tfix}^{\text {d }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} \mathrm{L}-1,6 \\ (\mathrm{~L}-41) \end{gathered}$ | $\begin{aligned} & \mathrm{L}-2.5 \\ & (\mathrm{~L}-64) \end{aligned}$ | $\begin{aligned} & \mathrm{L}-2.5 \\ & (\mathrm{~L}-64) \end{aligned}$ | $\begin{aligned} & \mathrm{L}-3.25 \\ & (\mathrm{~L}-.83) \end{aligned}$ | $\begin{gathered} \mathrm{L}-3 \\ (\mathrm{~L}-76) \end{gathered}$ | $\begin{aligned} & \mathrm{L}-4.25 \\ & (\mathrm{~L}-108) \end{aligned}$ | $\begin{aligned} & \mathrm{L}-3.25 \\ & \text { (L-83) } \end{aligned}$ | $\begin{gathered} \mathrm{L}-5 \\ (\mathrm{~L}-127) \end{gathered}$ | $\begin{gathered} \mathrm{L}-4 \\ (\mathrm{~L}-102) \end{gathered}$ | $\begin{aligned} & \mathrm{L}-6.25 \\ & (\mathrm{~L}-159) \end{aligned}$ |

For SI: 1 inch $=25.4 \mathrm{~mm}, 1 \mathrm{ft}-\mathrm{lb}=1.356 \mathrm{Nm}$.

1. The embedment depth, $h_{\text {nom, }}$, is measured from the outside surface of the concrete member to the embedded end of the anchor.
2. The listed minimum overall anchor length is based on anchor sizes commercially available at the time of publication compared with the requirements to achieve the minimum nominal embedment depth and possible fixture attachment.
3. Caution: holes in metal fixtures to be mounted should match the diameter specified in the table below.
4. Caution: oversized holes in base material will reduce or eliminate the mechanical interlock of the threads with the base material and reduce the anchor's load capacity
5. Caution: reuse of the anchor to achieve listed load values is not recommended

## TDE / TLE

## 3. PRODUCT INSTALLATION IN CONCRETE



## 1. DRILL

Drill a hole into the base material of the correct diameter and depth using a drill bit that meets the requirements of ANSI B212.15
Caution: oversized holes in base material will reduce or eliminate the mechanical interlock of the threads with the base material and reduce the anchor's load capacity


## 2. BLOW AND CLEAN

Remove dust and debris from hole using a hand pump, compressed air or a vacuum to remove loose particles left from drilling.


## 3. INSTALL

Select a powered impact wrench or a torque wrench that does not exceed the maximum torque $\mathrm{T}_{\text {impact,max }}$ or $\mathrm{T}_{\text {ins,max }}$ respectively. Attach an appropriate sized hex socket to the wrench. Mount the screw anchor head in the socket.

## 4. APPLY TORQUE

Drive the anchor with an impact driver or a torque wrench through the fixture and into the hole until the anchor head washer comes in contact with the fixture. The anchor must be snug after installation. Do not spin the hex socket off the anchor to disengage.

The screw anchor is permitted to be loosened by a maximum of one full turn and retightened with a torque wrench or a powered impact wrench to facilitate fixture attachment or realignment

Installation accessories

| Code no. | Description | Box qty. | Image |
| :---: | :---: | :---: | :---: |
| MOBOMBA | Hand pump / Dust blower. | 1 |  |
| MORCEPKIT | Kit 3 cleaning brushes | 1 |  |

## 4. DESIGN INFORMATION FOR CONCRETE APPLICATIONS

## Tension design information ${ }^{1,2}$

| Design characteristic |  | Notation | Units | Nominal anchor diameter |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1/4" |  | 3/8" |  | 1/2" |  | 5/8" |  | 3/4" |  |
| Nominal embedment depth |  |  | $\mathrm{h}_{\text {nom }}$ | $\begin{gathered} \mathrm{in}^{(\mathrm{mm})} \end{gathered}$ | $\begin{aligned} & 15 / 8 \\ & (41) \end{aligned}$ | $\begin{array}{r} 21 / 2 \\ (64) \end{array}$ | $\begin{aligned} & 21 / 2 \\ & (64) \end{aligned}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{aligned} & 41 / 4 \\ & (108) \end{aligned}$ | $\begin{aligned} & 31 / 4 \\ & (83) \end{aligned}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & 61 / 4 \\ & (159) \end{aligned}$ |
| Anchor category |  | 1, 2 or 3 | - | 2 |  | 1 |  | 1 |  | 1 |  | 1 |  |
| STEEL STRENGTH IN TENSION (ACl 318-14 17.4.1 or ACl 318-11 D.5.1) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum specified ultimate strength |  | $f_{\text {uta }}$ | $\begin{array}{\|c\|} \hline \mathrm{psi} \\ \left(\mathrm{~N} / \mathrm{mm}^{2}\right) \\ \hline \end{array}$ | $\begin{gathered} 110.000 \\ (758) \end{gathered}$ |  | $\begin{gathered} 111,000 \\ (765) \end{gathered}$ |  | $\begin{gathered} 107,000 \\ (738) \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline 102,000 \\ (703) \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline 99,000 \\ (683) \\ \hline \end{gathered}$ |  |
| Minimum specified yield strength |  | $\mathrm{fy}_{y}$ | $\begin{gathered} \mathrm{psi} \\ \left(\mathrm{~N} / \mathrm{mm}^{2}\right) \end{gathered}$ | $\begin{gathered} 88.000 \\ (607) \\ \hline \end{gathered}$ |  | $\begin{gathered} 88,800 \\ (612) \end{gathered}$ |  | $\begin{gathered} 85,600 \\ (590) \end{gathered}$ |  | $\begin{gathered} 81,600 \\ (563) \\ \hline \end{gathered}$ |  | $\begin{gathered} 79,200 \\ (546) \end{gathered}$ |  |
| Effective tensile stress area (screw anchor body) |  | $\mathrm{A}_{\mathrm{se}, \mathrm{N}}$ | $\begin{gathered} \mathrm{in}^{2} \\ \left(\mathrm{~mm}^{2}\right) \end{gathered}$ | $\begin{aligned} & 0.0438 \\ & (28,3) \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 0.0943 \\ & (60.8) \end{aligned}$ |  | $\begin{aligned} & 0.1768 \\ & (114.1) \end{aligned}$ |  | $\begin{aligned} & 0.2703 \\ & (174.4) \end{aligned}$ |  | $\begin{aligned} & 0.3988 \\ & (257.3) \end{aligned}$ |  |
| Steel strength in tension ${ }^{3}$ |  | $\mathrm{N}_{\text {sa }}$ | $\begin{gathered} \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{aligned} & 4,820 \\ & (21,4) \end{aligned}$ |  | $\begin{gathered} 10,467 \\ (46.6) \end{gathered}$ |  | $\begin{gathered} 18,918 \\ (84.1) \end{gathered}$ |  | $\begin{aligned} & \hline 27,571 \\ & (122.6) \end{aligned}$ |  | $\begin{aligned} & 39,481 \\ & (175.6) \end{aligned}$ |  |
| Strength reduction factor for steel failure in tension ${ }^{4}$ |  | $\phi_{\text {sa }}$ | - | 0.65 |  |  |  |  |  |  |  |  |  |
| PULLOUT STRENGTH IN TENSION (ACl 318-14 17.4.3 or ACl 318-11 D.5.3) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Characteristic pullout strength, uncracked concrete ( $2,500 \mathrm{psi})^{6,7}$ |  | $\mathrm{N}_{\mathrm{p}, \text { uncr }}$ | $\begin{gathered} \text { lb } \\ (\mathrm{kN}) \end{gathered}$ | $\begin{aligned} & 1,600 \\ & (7.12) \\ & \hline \end{aligned}$ | $\begin{gathered} 3,345 \\ (14.87) \end{gathered}$ | - | - | - | - | - | - | - | - |
| Characteristic pullout strength, cracked concrete ( $2,500 \mathrm{psi})^{6,7}$ |  | $\mathrm{N}_{\mathrm{p}, \mathrm{cr}}$ | $\begin{gathered} \hline \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{gathered} 730 \\ (3.26) \\ \hline \end{gathered}$ | $\begin{aligned} & 1,330 \\ & (5.91) \end{aligned}$ | - | - | $\begin{gathered} 3,223 \\ (14.33) \\ \hline \end{gathered}$ | - | - | - | - | - |
| Characteristic pullout strength, cracked concrete ( $2,500 \mathrm{psi}$ ), sesimic ${ }^{6,7,8}$ |  | $\mathrm{N}_{\mathrm{p}, \mathrm{eq}}$ | $\begin{gathered} \hline \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{gathered} 730 \\ (3.26) \\ \hline \end{gathered}$ | $\begin{aligned} & 1,330 \\ & (5.91) \end{aligned}$ | - | - | $\begin{gathered} 3,223 \\ (14.33) \end{gathered}$ | - | - | - | - | - |
| Normalization exponent | Uncracked concrete | n | - | 0,42 | 0,37 | - | - | 0.50 | - | - | - | - | - |
|  | Cracked concrete | n | - | 0,39 | 0,50 | - | - | 0,35 | - | - | - | - | - |
| Strength reduction factor for pullout strength in tension ${ }^{4}$ |  | $\phi_{\text {cb }}$ | - | 0.55 |  | 0.65 |  |  |  |  |  |  |  |
| CONCRETE BREAKOUT STRENGTH IN TENSION (ACl 318-14 17.4.2 or ACl 318-11 D.5.2) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Effective embedment |  | $h_{\text {ef }}$ | $\begin{aligned} & \text { in } \\ & (\mathrm{mm}) \end{aligned}$ | $\begin{aligned} & \hline 1,23 \\ & (31) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,98 \\ & (50) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.85 \\ & (47) \end{aligned}$ | $\begin{aligned} & 2.49 \\ & (63) \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.21 \\ & (56) \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.27 \\ & (83) \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.36 \\ & (60) \end{aligned}$ | $\begin{aligned} & 3.85 \\ & (98) \end{aligned}$ | $\begin{aligned} & 2.97 \\ & (75) \end{aligned}$ | $\begin{array}{r} \hline 4.89 \\ (124) \\ \hline \end{array}$ |
| Effectiveness factor for uncracked concrete ${ }^{9}$ |  | $\mathrm{k}_{\text {uncr }}$ | - | 24 | 24 | 27 | 27 | 27 | 24 | 24 | 24 | 24 | 24 |
| Effectiveness factor for cracked concrete ${ }^{9}$ |  | $\mathrm{k}_{\mathrm{cr}}$ | - | 17 | 17 | 17 | 17 | 21 | 17 | 17 | 17 | 17 | 17 |
| Critical edge distance |  | Cac | $\begin{gathered} \mathrm{in} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{aligned} & 33 / 4 \\ & (95) \end{aligned}$ | $\begin{gathered} 7 \\ (178) \end{gathered}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{gathered} 8 \\ (203) \end{gathered}$ |
| Strength reduction factor for pullout strength in tension ${ }^{4}$ |  | $\phi_{p}$ | - | 0.55 |  | 0.65 |  |  |  |  |  |  |  |
| Axial stiffness in service load range | Uncracked concrete | $\beta$ uncr | $\begin{array}{\|c\|} \hline \mathrm{lb} / \mathrm{in} \\ (\mathrm{kN} / \mathrm{mm}) \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 214,520 \\ (37,570) \\ \hline \end{array}$ | $\begin{array}{\|l} \hline 178,090 \\ (31,190) \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline 63,150 \\ (11,059) \\ \hline \end{array}$ | $\begin{aligned} & 207,850 \\ & (36,400) \end{aligned}$ | $\begin{aligned} & 139,250 \\ & (24,386) \end{aligned}$ | $\begin{aligned} & 140,060 \\ & (24,528) \end{aligned}$ | $\begin{aligned} & 222,870 \\ & (39,031) \\ & \hline \end{aligned}$ | $\begin{aligned} & 254,980 \\ & (44,653) \\ & \hline \end{aligned}$ | $\begin{aligned} & 292,630 \\ & (51,247) \\ & \hline \end{aligned}$ | $\begin{array}{\|l} 305,530 \\ (53,506) \\ \hline \end{array}$ |
|  | Cracked concrete | $\beta$ cr | $\begin{gathered} \mathrm{lb} / \mathrm{in} \\ (\mathrm{kN} / \mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 186,270 \\ & (32,620) \\ & \hline \end{aligned}$ | $\begin{aligned} & 178,950 \\ & (31,340) \end{aligned}$ | $\begin{gathered} 63,150 \\ (11,059) \end{gathered}$ | $\begin{aligned} & 174,020 \\ & (30,476) \end{aligned}$ | $\begin{aligned} & 130,385 \\ & (22,834) \end{aligned}$ | $\begin{aligned} & 140,060 \\ & (24,528) \end{aligned}$ | $\begin{aligned} & 105,130 \\ & (18,411) \end{aligned}$ | $\begin{aligned} & 192,280 \\ & (33,673) \end{aligned}$ | $\begin{aligned} & 160,050 \\ & (28,029) \end{aligned}$ | $\begin{aligned} & 165,525 \\ & (28,968) \end{aligned}$ |

For SI: $1 \mathrm{inch}=25.4 \mathrm{~mm}, 1 \mathrm{in}^{2}=645 \mathrm{~mm}^{2}, 1 \mathrm{psi}=0,00689 \mathrm{~N} / \mathrm{mm}^{2} ; 1 \mathrm{lb}=0,00445 \mathrm{kN}, 1 \mathrm{lbf} / \mathrm{in}=0,175 \mathrm{kN} / \mathrm{mm}$

1. The data in this table is intended to be used with the design provisions of ACl 318-14 Chapter 17 or ACI 318 Appendix D , as applicable; for anchors resisting seismic load combinations the additional requirements of $\mathrm{ACl} 318-1417.2$.3 or ACl 318 D.3.3, as applicable, shall apply.
2. Installation must comply with published instructions and details.
3. Tabulated values for steel strength in tension are based on test results per ACI 355.2 and must be used for design.
4. All values of $\phi$ were determined from the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2, as applicable. If the load combinations of ACI 318-11 Appendix C are used, then the appropriate value of $\phi$ must be determined in accordance with ACI 318-11 D.4.4. For reinforcement that meets $\mathrm{ACI} 318-14 \mathrm{Chapter} 17$ or ACI 318 Appendix D, as applicable, requirements for Condition A, see ACI 318-14 17.3.3 or ACI 318-11 D.4.3, as applicable, for the appropriate $\phi$ factor when the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3 or ACI 318-11 Section 9.2, as applicable, are used
5. TDE / TLE screw anchor is considered a brittle steel element in tension as defined by $\mathrm{ACI} 318-142.3$ or ACI 318 D .1 , as applicable.
6. For concrete compressive strength greater than $2,500 \mathrm{psi}, \mathrm{N}_{\mathrm{pn}}=\left(\right.$ pullout strength value from table)*${ }^{*}(\text { specified concrete compressive strength } / 2500)^{n}$
7. 
8. Pullout strength does not control design of indicated anchors. Do not calculate pullout strength for indicated anchor size and embedment
9. Reported values for characteristic pullout strength in tension for seismic applications are based on test results per ACI 355.2 , Section 9.5
10. Select appropriate effectiveness factor for cracked concrete ( $\mathrm{k}_{\mathrm{cr}}$ ) or uncracked concrete ( $\mathrm{k}_{\mathrm{ucr}}$ ).
11. Mean values shown; actual stiffness varies considerable depending on concrete strength, loading and geometry of application
12. Anchors are permitted to be used in sand-lightweight concrete provided that $N_{\mathrm{b}}, \mathrm{N}_{\mathrm{eq}}$ and $\mathrm{N}_{\mathrm{pn}}$ are multiplied by a factor of 0.60 .

## Shear design information ${ }^{1,2}$

| Design characteristic | Notation | Units | Nominal anchor diameter |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1/4" |  | 3/8" |  | 1/2" |  | 5/8" |  | 3/4" |  |
| Nominal embedment depth | $\mathrm{h}_{\text {nom }}$ | $\begin{gathered} \mathrm{in}^{(\mathrm{mm})} \end{gathered}$ | $\begin{aligned} & 15 / 8 \\ & (41) \end{aligned}$ | $\begin{aligned} & 21 / 2 \\ & (64) \end{aligned}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{aligned} & 41 / 4 \\ & (108) \end{aligned}$ | $\begin{aligned} & 3 \text { 1/4 } \\ & (83) \end{aligned}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & 61 / 4 \\ & (159) \end{aligned}$ |
| Anchor category | 1, 2 or 3 | - |  | 2 |  |  |  |  |  |  |  |  |
| STEEL STRENGTH IN SHEAR (ACl 318-14 17.5.1 or ACl 318-11 D.6.1) ${ }^{5}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum specified ultimate strength | $f_{\text {uta }}$ | $\begin{gathered} \mathrm{psi} \\ \left(\mathrm{~N} / \mathrm{mm}^{2}\right) \end{gathered}$ | $\begin{gathered} 110.000 \\ (758) \end{gathered}$ |  | $\begin{gathered} 111,000 \\ (765) \end{gathered}$ |  | $\begin{gathered} 107,000 \\ (738) \end{gathered}$ |  | $\begin{gathered} 102,000 \\ (703) \end{gathered}$ |  | $\begin{gathered} 99,000 \\ (683) \end{gathered}$ |  |
| Minimum specified yield strength | $\mathrm{fy}_{y}$ | $\begin{gathered} \mathrm{psi} \\ \left(\mathrm{~N} / \mathrm{mm}^{2}\right) \end{gathered}$ | $\begin{gathered} 88.000 \\ (607) \end{gathered}$ |  | $\begin{gathered} 88,800 \\ (612) \end{gathered}$ |  | $\begin{gathered} 85,600 \\ (590) \end{gathered}$ |  | $\begin{gathered} 81,600 \\ (563) \end{gathered}$ |  | $\begin{gathered} 79,200 \\ (546) \end{gathered}$ |  |
| Effective tensile stress area (screw anchor body) | $\mathrm{A}_{\text {se, }, ~}$ | $\begin{gathered} \mathrm{in}^{2} \\ \left(\mathrm{~mm}^{2}\right) \end{gathered}$ | $\begin{aligned} & 0.0438 \\ & (28,3) \end{aligned}$ |  | $\begin{aligned} & 0.0943 \\ & (60.8) \end{aligned}$ |  | $\begin{aligned} & 0.1768 \\ & (114.1) \end{aligned}$ |  | $\begin{aligned} & 0.2703 \\ & (174.4) \end{aligned}$ |  | $\begin{aligned} & 0.3988 \\ & (257.3) \end{aligned}$ |  |
| Steel strength in shear ${ }^{3}$ | $\mathrm{V}_{\text {sa }}$ | $\begin{gathered} \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{aligned} & 1,555 \\ & (6,92) \end{aligned}$ | $\begin{gathered} \hline 2,738 \\ (12.18) \end{gathered}$ | $\begin{gathered} \hline 4,817 \\ (21.43) \end{gathered}$ | $\begin{gathered} \hline 4,848 \\ (21.57) \end{gathered}$ | $\begin{gathered} \hline 7,268 \\ (32.33) \end{gathered}$ | $\begin{gathered} 9,371 \\ (41.68) \end{gathered}$ | $\begin{array}{\|l\|} \hline 10,300 \\ (45.81) \end{array}$ | $\begin{aligned} & 12,736 \\ & (56.65) \end{aligned}$ | $\begin{aligned} & 14,238 \\ & (63.33) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 14,238 \\ & (63.33) \\ & \hline \end{aligned}$ |
| Steel strength in shear, seismic (2500 psi) ${ }^{5}$ | $\mathrm{V}_{\text {sa, eq }}$ | $\begin{gathered} \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{aligned} & 1,555 \\ & (6,92) \end{aligned}$ | $\begin{gathered} \hline 2,493 \\ (11,09) \end{gathered}$ | $\begin{aligned} & 4,075 \\ & (18.13 \end{aligned}$ | $\begin{array}{\|c\|} \hline 4,075 \\ (18.13) \end{array}$ | $\begin{gathered} \hline 5,075 \\ (22.57) \end{gathered}$ | $\begin{array}{\|c} \hline 7,142 \\ (31.77) \end{array}$ | $\begin{array}{\|c} \hline 8,029 \\ (35.72) \end{array}$ | $\begin{aligned} & 10,302 \\ & (45.83) \end{aligned}$ | $\begin{aligned} & 12,105 \\ & (53.85) \end{aligned}$ | $\begin{aligned} & 12,105 \\ & (53.85) \end{aligned}$ |
| Strength reduction factor for steel failure in shear ${ }^{6}$ | $\phi_{\text {sa }}$ | - | 0.60 |  |  |  |  |  |  |  |  |  |
| CONCRETE BREAKOUT STRENGTH IN SHEAR (ACl 318-14 17.5.2 or ACl 318-11 D.6.2) |  |  |  |  |  |  |  |  |  |  |  |  |
| Nominal anchor diameter | $\mathrm{d}_{0}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 1 / 4 \\ (6,4) \\ \hline \end{gathered}$ | $\begin{gathered} 1 / 4 \\ (6,4) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 8 \\ (9.5) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 8 \\ (9.5) \\ \hline \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \\ \hline \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3 / 4 \\ (19.1) \\ \hline \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \\ \hline \end{gathered}$ |
| Load bearing length of anchor | le | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 1,23 \\ & (31) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,98 \\ & (50) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.85 \\ & (47) \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.49 \\ & (63) \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.21 \\ & (56) \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.27 \\ & (83) \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.36 \\ & (60) \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.85 \\ & (98) \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.97 \\ & 75) \\ & \hline \end{aligned}$ | $\begin{array}{r} 4.89 \\ (124) \\ \hline \end{array}$ |
| Strength reduction factor for concrete strength in shear ${ }^{6}$ | $\phi_{\text {cb }}$ | - | 0.70 |  |  |  |  |  |  |  |  |  |
| PRYOUT STRENGTH IN SHEAR (ACl 318-14 17.5.3 or ACl 318-11 D.6.3) |  |  |  |  |  |  |  |  |  |  |  |  |
| Coefficient for pryout strength | $\mathrm{k}_{\mathrm{cp}}$ | - | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 2.0 | 1.0 | 2.0 | 2.0 | 2.0 |
| Effective embedment depth | $h_{\text {ef }}$ | $\begin{gathered} \hline \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & \hline 1,23 \\ & (31) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,98 \\ & (50) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1.85 \\ & (47) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.49 \\ & (63) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.21 \\ & (56) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.27 \\ & (83) \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.36 \\ & (60) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.85 \\ & (98) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.97 \\ & (75) \\ & \hline \end{aligned}$ | $\begin{array}{r} 4.89 \\ (124) \\ \hline \end{array}$ |
| Reduction factor for pryout strength in shear ${ }^{6}$ | $\phi_{\text {cp }}$ | - | 0.70 |  |  |  |  |  |  |  |  |  |

For SI: 1 inch $=25.4 \mathrm{~mm}, 1 \mathrm{in}^{2}=645 \mathrm{~mm}^{2}, 1 \mathrm{psi}=0,00689 \mathrm{~N} / \mathrm{mm}^{2} ; 1 \mathrm{lb}=0,00445 \mathrm{kN}$

1. The data in this table is intended to be used with the design provisions of $\mathrm{ACl} 318-14$ Chapter 17 or ACl 318 Appendix D , as applicable; for anchors resisting seismic load combinations the additional requirements of $\mathrm{ACl} 318-1417.2 .3$ or ACI 318 D .3 .3 shall apply, as applicable.
Installation must comply with published instructions and details.
2. Reported values for steel strength in shear are based on test results per ACI 355.2 , Section 9.4 and shall be used for design.
3. TDE / TLE is considered a brittle steel element as defined by ACI 318-14 2.3 or ACI 318-11 D.1, as applicable.
4. Reported values for steel strength in shear for seismic applications are based on test results per ACI 355.2, Section 9.6
5. All values of $\phi$ were determined from the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3 or ACI 318 Section 9.2 . If the load combinations of ACI 318-11 Appendix C are used, then the appropriate value of $\Phi$ must be determined in accordance with ACI 318-11 D.4.4. For reinforcement that meets ACI 318-14 Chapter 17 or ACI 318-11 Appendix D, as applicable, requirements for Condition A, see ACI 318-14 17.3.3 or ACI 318-11 D.4.3, for the appropriate $\phi$ factor when the load combinations of IBC Section 1605.2, ACI 318-14 Section 5.3 or ACI 318 Section 9.2 are used.
6. Anchors are permitted to be used in sand-lightweight concrete provided that $\mathrm{V}_{\mathrm{b}}$ and $\mathrm{V}_{\mathrm{cp}}$ are multiplied by a factor of 0.60 .

## TDE / TLE

Factored design strength ( $\Phi \mathrm{N}_{\mathrm{n}}$ and $\Phi \mathrm{V}_{\mathrm{n}}$ ) calculated in accordance with ACI 318-14:
1- Tabular values are provided for illustration and are applicable for single anchors installed in normal weight concrete with minimum slab thickness, $h_{a}=h_{\text {min }}$, and with the following conditions:
$\mathrm{C}_{a 1}$ is greater than or equal to the critical edge distance, $\mathrm{C}_{a c}$ (table values based on $\mathrm{C}_{a 1}=\mathrm{C}_{a c}$ ).
$\mathrm{C}_{\mathrm{a} 2}$ is greater than or equal to 1.5 times $\mathrm{C}_{\mathrm{a} 1}$.
2- Calculations were performed according to $\mathrm{ACI} 318-14$. The load level corresponding to the controlling failure mode is listed. (e.g. For tension: steel, concrete breakout and pullout; For shear: steel, concrete breakout and pryout). Furthermore, the capacities for concrete breakout strength in tension and pryout strength in shear are calculated using the effective embedment values, $\mathrm{h}_{\mathrm{ef}}$, for the selected anchors as noted in the design information tables. Please also reference the installation specifications for more information.
3 - $\quad$ Strength reduction factors $(\Phi)$ were based on $\mathrm{ACI} 318-14$ section 17.3 .3 for load combinations. Condition $B$ is assumed. Condition $B$ is applied where supplementary reinforcement is not supplied.
4- Tabular values are permitted for static loads only, seismic loading is not considered with these tables.
5- For designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318-14 section 17.6.
6- Interpolation is not permitted to be used with the tabular values. For intermediate base material compressive strengths please see ACI 318-14. For other design conditions including seismic considerations please see $\mathrm{ACI} 318-14$.

## Tension and shear design strengths for TDE / TLE in cracked concrete



## Tension and shear design strengths for TDE / TLE in uncracked concrete

| Nominal anchor diameter (in.) | Nominal embed. $h_{\text {nom }}$ (in.) | Minimum concrete compressive strength |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}^{\prime}=2,500 \mathrm{psi}$ |  | $\mathrm{f}^{\prime}{ }_{\text {c }}=3,000 \mathrm{psi}$ |  | $\mathrm{f}^{\prime}=4,000 \mathrm{psi}$ |  | $\mathrm{f}^{\prime} \mathrm{c}=6,000 \mathrm{psi}$ |  | $\mathrm{f}^{\prime}{ }_{\mathrm{c}}=8,000 \mathrm{psi}$ |  |
|  |  | $\begin{gathered} \Phi \mathrm{N}_{\mathrm{n}} \\ \text { Tension } \\ \text { (lb.) } \\ \hline \end{gathered}$ | $\Phi V_{n}$ Shear (lb.) | $\Phi \mathrm{N}_{\mathrm{n}}$ Tension (lb.) | $\Phi V_{n}$ Shear (lb.) | $\Phi \mathrm{N}_{\mathrm{n}}$ Tension (lb.) | $\Phi V_{n}$ Shear (lb.) | $\Phi \mathrm{N}_{\mathrm{n}}$ Tension (lb.) | $\Phi \mathrm{V}_{\mathrm{n}}$ Shear (lb.) | $\Phi \mathrm{N}_{\mathrm{n}}$ Tension (lb.) | $\Phi V_{n}$ Shear (lb.) |
| 1/4 | $15 / 8$ | 881 | 933 | 915 | 933 | 973 | 933 | 1,059 | 933 | 1,125 | 933 |
|  | $21 / 2$ | 1,839 | 1,643 | 1,902 | 1,643 | 2,006 | 1,643 | 2,162 | 1,643 | 2,280 | 1,643 |
| 3/8 | $21 / 2$ | 2.208 | 2.378 | 2.419 | 2.605 | 2.793 | 2.890 | 3.421 | 2.890 | 3.950 | 2.890 |
|  | $31 / 4$ | 3.448 | 2.909 | 3.777 | 2.909 | 4.361 | 2.909 | 5.341 | 2.909 | 6.168 | 2.909 |
| 1/2 | 3 | 2.883 | 3.105 | 3.158 | 3.401 | 3.647 | 3.927 | 4.466 | 4.361 | 5.157 | 4.361 |
|  | $41 / 4$ | 4.612 | 5.623 | 5.053 | 5.623 | 5.834 | 5.623 | 7.145 | 5.623 | 8.251 | 5.623 |
| 5/8 | $31 / 4$ | 2.828 | 3.045 | 3.098 | 3.336 | 3.577 | 3.852 | 4.381 | 4.718 | 5.059 | 5.448 |
|  | 5 | 5.892 | 7.642 | 6.455 | 7.642 | 7.453 | 7.642 | 9.128 | 7.642 | 10.540 | 7.642 |
| 3/4 | 4 | 3.992 | 8.543 | 4.373 | 8.543 | 5.050 | 8.543 | 6185 | 8.543 | 7.142 | 8.543 |
|  | $61 / 4$ | 8.434 | 8.543 | 9.240 | 8.543 | 10.669 | 8.543 | 13.067 | 8.543 | 15.088 | 8.543 |
| Color code: |  |  | Pullout $\square$ Concrete / pryout | Concrete / pryout |  |  |  | Steel |  |  |  |

## Converted allowable loads for TDE /TLE

ESR-4314 provides design information for load factor and characteristic resistance (LRFD), however allowable stress design (ASD) is still in use by some users. Translation of LRFD to ASD values is possible, however it is dependent on the levels of dead load and live load. Dead load is defined in the ACI 318 Building Code Requirements for Structural Concrete as "the weights of members, supported structure and permanent attachments that are likely to be present on a structure in service". Live load is defined in $\mathrm{ACl} 318-14$ as "load that is not permanently applied to a structure, but is likely to occur during the service life of the structure (excluding environmental loads)". Examples of live loads are traffic on a walkway and non permanent loads associated with usage of a structure. Live load values are stipulated in the building code for various loading conditions and parts of structures.

To facilitate the translation of LRFD characteristic values to ASD values, a scenario of dead load and live load level is used to conservatively address the most common application as follows: 30\% dead load; 70\% live load. ACI 318-14 Equation (5.3.1b) provides a conversion factor of 1,48 which is divided into the LRFD characteristic resistances and multiplied by a $\phi$ factor (according to the failure type) to determine an equivalent ASD load.

It is the responsibility of the user to select the appropriate ASD values based on the example loadings shown in this document or alternative dead versus live loading that may be applicable to the specific design.

The ASD values are provided in the following tables for tension and shear for different concrete strengths. Other installation and design provisions in ESR-4314 must be followed.

Converted allowable loads for TDE /TLE in cracked concrete

| Nominal anchor diameter (in.) | Nominal embed. $h_{\text {nom }}$ (in.) | Minimum concrete compressive strength |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}_{\mathrm{c}}^{\prime}=2,500 \mathrm{psi}$ |  | $\mathrm{f}^{\prime}{ }_{\text {c }}=3,000 \mathrm{psi}$ |  | $\mathrm{f}_{\mathrm{c}}{ }^{\text {a }}$ 4,000 psi |  | $\mathrm{f}_{\mathrm{c}} \mathbf{=}=6,000 \mathrm{psi}$ |  | $\mathrm{f}^{\prime}{ }_{c}=8,000 \mathrm{psi}$ |  |
|  |  | $\mathrm{T}_{\text {allowable ASD }}$ <br> Tension (lb) | $\begin{aligned} & V_{\text {allowable ASD }} \\ & \text { Shear (Ib) } \\ & \hline \end{aligned}$ | $\mathrm{T}_{\text {allowable ASD }}$ <br> Tension (lb) | $\begin{aligned} & V_{\text {allowable ASD }} \\ & \text { Shear (Ib) } \end{aligned}$ | Tallowable ASD <br> Tension (lb) | $\begin{aligned} & V_{\text {allowable ASD }} \\ & \text { Shear (Ib) } \\ & \hline \end{aligned}$ | Tallowable ASD <br> Tension (lb) | $\begin{aligned} & V_{\text {allowable ASD }} \\ & \text { Shear (Ib) } \end{aligned}$ | $\mathrm{T}_{\text {allowable ASD }}$ <br> Tension (lb) | $\begin{aligned} & V_{\text {allowable ASD }} \\ & \text { Shear (Ib) } \end{aligned}$ |
| 1/4 | $15 / 8$ | 272 | 548 | 282 | 601 | 298 | 630 | 323 | 630 | 341 | 630 |
|  | $21 / 2$ | 494 | 1,110 | 517 | 1,110 | 555 | 1,110 | 614 | 1,110 | 660 | 1,110 |
| 3/8 | $21 / 2$ | 939 | 1.012 | 1.029 | 1.108 | 1.188 | 1.280 | 1.455 | 1.567 | 1.680 | 1.810 |
|  | $31 / 4$ | 1.467 | 1.580 | 1.607 | 1.730 | 1.855 | 1.965 | 2.272 | 1.965 | 2.624 | 1.965 |
| 1/2 | 3 | 1.415 | 1.632 | 1.461 | 1.787 | 1.537 | 2.064 | 1.650 | 2.528 | 1.735 | 2.919 |
|  | $41 / 4$ | 2.207 | 3.779 | 2.418 | 3.779 | 2.792 | 3.779 | 3.420 | 3.779 | 3.949 | 3.779 |
| 5/8 | $31 / 4$ | 1.353 | 1.458 | 1.483 | 1.597 | 1.712 | 1.844 | 2.097 | 2.258 | 2.421 | 2.607 |
|  | 5 | 2.820 | 5.163 | 3.089 | 5.163 | 3.587 | 5.163 | 4.369 | 5.163 | 5.045 | 5.163 |
| 3/4 | 4 | 1.911 | 4.115 | 2.093 | 4.508 | 2.417 | 5.206 | 2.960 | 5.772 | 3.418 | 5.772 |
|  | $61 / 4$ | 4.037 | 5.772 | 4.422 | 5.772 | 5.106 | 5.772 | 6.254 | 5.772 | 7.221 | 5.772 |

1. Allowable load values are calculated using a conversion factor, $\alpha$, from factored design strengths.
2. Tabulated allowable load values assume $30 \%$ dead load and $70 \%$ live load, with controlling load combination $1,2 \mathrm{D}+1,6 \mathrm{~L}$. Calculated weighted average for the conversion factor, $\alpha=1,2^{\star}(0,3)+1,6^{\star}(0,7)=1,48$.

Converted allowable loads for TDE in uncracked concrete

| Nominal anchor diameter (in.) | Nominal embed. $h_{\text {nom }}$ (in.) | Minimum concrete compressive strength |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{f}^{\prime}{ }^{\text {a }}$ 2,500 psi |  | $\mathrm{f}^{\prime}{ }_{c}=3,000 \mathrm{psi}$ |  | $\mathrm{f}_{\mathrm{c}}{ }^{\text {c }}$ 4,000 psi |  | $\mathrm{f}_{\mathrm{c}}^{\prime}=6,000 \mathrm{psi}$ |  | $\mathrm{f}^{\prime}{ }_{\mathrm{c}}=8,000 \mathrm{psi}$ |  |
|  |  | $\mathrm{T}_{\text {allowable ASD }}$ <br> Tension (lb) | Vallowable ASD <br> Shear (lb) | Tallowable ASD <br> Tension (lb) | Vallowable ASD <br> Shear (lb) | Tallowable ASD <br> Tension (lb) | $V_{\text {allowable ASD }}$ <br> Shear (lb) | Tallowable ASD <br> Tension (lb) | Vallowable ASD <br> Shear (lb) | Tallowable ASD <br> Tension (lb) | $V_{\text {allowable ASD }}$ <br> Shear (Ib) |
| 1/4 | $15 / 8$ | 595 | 630 | 619 | 630 | 657 | 630 | 715 | 630 | 760 | 630 |
|  | $21 / 2$ | 1,242 | 1,110 | 1,285 | 1,110 | 1,355 | 1,110 | 1,461 | 1,110 | 1,541 | 1,110 |
| 3/8 | $21 / 2$ | 1.492 | 1.607 | 1.634 | 1760 | 1.887 | 1.953 | 2.311 | 2.116 | 2.669 | 1.953 |
|  | $31 / 4$ | 2.330 | 1.965 | 2.552 | 1.965 | 2.947 | 1.965 | 3.609 | 1.965 | 4.167 | 1.965 |
| 1/2 | 3 | 1.948 | 2.098 | 2.134 | 2.298 | 2.464 | 2.653 | 3.018 | 2.947 | 3.485 | 2.947 |
|  | $41 / 4$ | 3.116 | 3.799 | 3.414 | 3.799 | 3.942 | 3.799 | 4.828 | 3.799 | 5.575 | 3.799 |
| 5/8 | $311 / 4$ | 1.911 | 2.058 | 2.093 | 2.254 | 2.417 | 2.603 | 2.960 | 3.188 | 3.418 | 3.681 |
|  | 5 | 3.981 | 5.165 | 4.361 | 5.165 | 5.036 | 5.165 | 6.168 | 5.165 | 7.122 | 5.165 |
| 3/4 | 4 | 2.698 | 5.772 | 2.955 | 5.772 | 3.412 | 5.772 | 4.179 | 5.772 | 4.826 | 5.772 |
|  | $61 / 4$ | 5.699 | 5.772 | 6.243 | 5.772 | 7.209 | 5.772 | 8.829 | 5.772 | 10.195 | 5.772 |

[^0]
## 5. INSTALLATION DETAILS IN GROUTED CMU MASONRY



| Parameter | Symbol | Units | Nominal anchor diameter |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1/4" |  | 3/8" |  | 1/2" |  | 5/8" |  | 3/4" |  |
| Drill bit diameter | $\mathrm{d}_{0}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 1 / 4 \\ (6.4) \end{gathered}$ | $\begin{array}{r} 1 / 4 \\ (6.4) \end{array}$ | $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ |
| Nominal embedment depth ${ }^{1}$ | hnom | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 15 / 8 \\ & (41) \end{aligned}$ | $\begin{array}{r} 21 / 2 \\ (64) \end{array}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{aligned} & 41 / 4 \\ & (108) \end{aligned}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & 61 / 4 \\ & (159) \end{aligned}$ |
| Effective embedment depth | $h_{\text {ef }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 1,23 \\ & (31) \end{aligned}$ | $\begin{aligned} & 1,98 \\ & (50) \end{aligned}$ | $\begin{aligned} & 1,42 \\ & (36) \end{aligned}$ | $\begin{aligned} & 2,49 \\ & (63) \end{aligned}$ | $\begin{aligned} & 1,78 \\ & (45) \end{aligned}$ | $\begin{aligned} & 3.27 \\ & (83) \end{aligned}$ | $\begin{aligned} & 2.36 \\ & (60) \end{aligned}$ | $\begin{aligned} & 3.85 \\ & (98) \end{aligned}$ | $\begin{aligned} & 2.97 \\ & (75) \end{aligned}$ | $\begin{aligned} & 4.89 \\ & (124) \end{aligned}$ |
| Minimum hole depth | $h_{\text {nole }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 27 / 8 \\ (73) \end{gathered}$ | $\begin{gathered} 23 / 8 \\ (60) \end{gathered}$ | $\begin{aligned} & 35 / 8 \\ & (92) \end{aligned}$ | $\begin{gathered} 27 / 8 \\ (73) \end{gathered}$ | $\begin{aligned} & 45 / 8 \\ & (117) \end{aligned}$ | $\begin{gathered} 35 / 8 \\ (92) \end{gathered}$ | $\begin{aligned} & 53 / 8 \\ & (137) \end{aligned}$ | $\begin{aligned} & 43 / 8 \\ & (111) \end{aligned}$ | $\begin{aligned} & 65 / 8 \\ & (168) \end{aligned}$ |
| Maximum fixture clearance Hole diameter | df | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | $\begin{gathered} 3 / 8 \\ (9.5) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 1 / 2 \\ (12.7) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} 5 / 8 \\ (15.9) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{gathered} 3 / 4 \\ (19.1) \end{gathered}$ | $\begin{gathered} 7 / 8 \\ (22.2) \end{gathered}$ | $\begin{gathered} 7 / 8 \\ (22.2) \end{gathered}$ |
| Maximum installation torque | Tinst | $\begin{gathered} \mathrm{ft} \mathrm{lb} \\ (\mathrm{Nm}) \end{gathered}$ | $\begin{gathered} 5 \\ (7) \end{gathered}$ | $\begin{gathered} 5 \\ (7) \end{gathered}$ | $\begin{gathered} 15 \\ (20) \end{gathered}$ | $\begin{gathered} 15 \\ (20) \end{gathered}$ | $\begin{gathered} 30 \\ (41) \end{gathered}$ | $\begin{gathered} 30 \\ (41) \end{gathered}$ | $\begin{gathered} 40 \\ (54) \end{gathered}$ | $\begin{gathered} 40 \\ (54) \end{gathered}$ | $\begin{gathered} 40 \\ (54) \end{gathered}$ | $\begin{gathered} 40 \\ (54) \end{gathered}$ |
| Maximum impact wrench torque rating | $T_{\text {impact.max }}$ | $\begin{gathered} \mathrm{ft} \mathrm{lb} \\ (\mathrm{Nm}) \end{gathered}$ | $\begin{gathered} 150 \\ (203) \end{gathered}$ | $\begin{gathered} 150 \\ (203) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{aligned} & 380 \\ & (515) \end{aligned}$ | $\begin{aligned} & 380 \\ & (515) \end{aligned}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ | $\begin{gathered} 380 \\ (515) \end{gathered}$ |
| Critical edge distance | Car | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 1,85 \\ & (47) \end{aligned}$ | $\begin{aligned} & 2,97 \\ & (75) \end{aligned}$ | $\begin{aligned} & 2,14 \\ & (54) \end{aligned}$ | $\begin{aligned} & 3,73 \\ & (95) \end{aligned}$ | $\begin{aligned} & 2,67 \\ & (68) \end{aligned}$ | $\begin{aligned} & 4,91 \\ & (125) \end{aligned}$ | $\begin{aligned} & 3,54 \\ & (90) \end{aligned}$ | $\begin{gathered} 5,78 \\ (147) \end{gathered}$ | $\begin{aligned} & 4,46 \\ & (113) \end{aligned}$ | $\begin{gathered} 7,34 \\ (186) \end{gathered}$ |
| Minimum distance to the head joint | $\mathrm{Cmmin}, \mathrm{h}, \mathrm{j}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ |
| Minimum edge distance field of wall | $\mathrm{Cmin}^{\text {m }}$ | $\begin{gathered} \text { in } \\ (m m) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 3 \\ (76) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ |
| Minimum spacing field of wall | $S_{\text {min }}$ | $\begin{aligned} & \text { in } \\ & (\mathrm{mm}) \end{aligned}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ |
| Minimum edge distance top of wall | Cmin | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ |
| Minimum spacing top of wall | $S_{\text {min }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{array}{r} 41 / 2 \\ (114) \end{array}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{array}{r} 41 / 2 \\ (114) \end{array}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{aligned} & 51 / 2 \\ & (140) \end{aligned}$ | $\begin{aligned} & 51 / 2 \\ & (140) \end{aligned}$ | $\begin{aligned} & 61 / 2 \\ & (165) \end{aligned}$ | $\begin{aligned} & 61 / 2 \\ & (165) \end{aligned}$ | $\begin{aligned} & 81 / 2 \\ & (216) \end{aligned}$ | $\begin{aligned} & 81 / 2 \\ & (216) \end{aligned}$ |
| Minimum overall anchor length ${ }^{2}$ | lanch | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 13 / 4 \\ & (44) \end{aligned}$ | $\begin{gathered} 25 / 8 \\ (67) \end{gathered}$ | $\begin{gathered} 21 / 4 \\ (57) \end{gathered}$ | $\begin{gathered} 31 / 2 \\ (89) \end{gathered}$ | $\begin{gathered} 23 / 4 \\ (82) \end{gathered}$ | $\begin{aligned} & 41 / 2 \\ & (114) \end{aligned}$ | $\begin{array}{r} 31 / 2 \\ (89) \end{array}$ | $\begin{aligned} & 51 / 4 \\ & (133) \end{aligned}$ | $\begin{aligned} & 41 / 4 \\ & (108) \end{aligned}$ | $\begin{aligned} & 61 / 2 \\ & (165) \end{aligned}$ |
| Spanner | Sw | in | 7/16 | 7/16 | 9/16 | 9/16 | 3/4 | 3/4 | 15/16 | 15/16 | $11 / 8$ | $11 / 8$ |
| Maximum fixture thickness | $\mathrm{t}_{\text {fix }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} \mathrm{L}-1,6 \\ (\mathrm{~L}-41) \end{gathered}$ | $\underset{(\mathrm{L}-64)}{\mathrm{L}-2.5}$ | $\begin{gathered} \mathrm{L}-2 \\ (\mathrm{~L}-51) \end{gathered}$ | $\begin{aligned} & \mathrm{L}-3.25 \\ & (\mathrm{~L}-.83) \end{aligned}$ | $\begin{aligned} & \mathrm{L}-2,5 \\ & (\mathrm{~L}-64) \end{aligned}$ | $\begin{aligned} & \mathrm{L}-4.25 \\ & (\mathrm{~L}-108) \end{aligned}$ | $\begin{aligned} & \text { L-3.25 } \\ & (\mathrm{L}-83) \end{aligned}$ | $\begin{gathered} \mathrm{L}-5 \\ (\mathrm{~L}-127) \end{gathered}$ | $\begin{gathered} \mathrm{L}-4 \\ (\mathrm{~L}-102) \end{gathered}$ | $\begin{aligned} & \mathrm{L}-6.25 \\ & (\mathrm{~L}-159) \end{aligned}$ |

For SI: 1 inch $=25.4 \mathrm{~mm}, 1 \mathrm{ft}-\mathrm{lb}=1.356 \mathrm{Nm}$.

1. The embedment depth, $h_{\text {nom }}$, is measured from the outside surface of the masonry member to the embedded end of the anchor.
2. The listed minimum overall anchor length is based on anchor sizes commercially available at the time of publication compared with the requirements to achieve the minimum nominal embedment depth and possible fixture attachment.
3. Caution: holes in metal fixtures to be mounted should match the diameter specified in the table below.
4. Caution: oversized holes in base material will reduce or eliminate the mechanical interlock of the threads with the base material and reduce the anchor's load capacity
5. Caution: reuse of the anchor to achieve listed load values is not recommended

## TDE / TLE

## 6. PRODUCT INSTALLATION IN CMU MASONRY



## 1. DRILL

Drill a hole into the base material of the correct diameter and depth using a drill bit that meets the requirements of ANSI B212.15

Caution: oversized holes in base material will reduce or eliminate the mechanical interlock of the threads with the base material and reduce the anchor's load capacity


## 2. BLOW AND CLEAN

Remove dust and debris from hole using a hand pump, compressed air or a vacuum to remove loose particles left from drilling.

## 3. INSTALL

Select a powered impact wrench or a torque wrench that does not exceed the maximum torque $\mathrm{T}_{\text {impact,max }}$ or $\mathrm{T}_{\text {ins,max }}$ respectively. Attach an appropriately sized hex socket to the wrench. Mount the screw anchor head in the socket.

## 4. APPLY TORQUE



Drive the anchor with an impact driver or a torque wrench through the fixture and into the hole until the anchor head washer comes in contact with the fixture. The anchor must be snug after installation. Do not spin the hex socket off the anchor to disengage.

The screw anchor is permitted to be loosened by a maximum of one full turn and retightened with a torque wrench or a powered impact wrench to facilitate fixture attachment or realignment

## Installation accessories

| Code no. | Description | Box qty. | Image |
| :---: | :---: | :---: | :---: |
| MOBOMBA | Hand pump / Dust blower. | 1 |  |
| MORCEPKIT | Kit 3 cleaning brushes | 1 |  |

## TDE / TLE

## Reference: FT TDE-en

## 7. DESIGN INFORMATION FOR CMU MASONRY APPLICATIONS

## Tension design information ${ }^{1,2}$

| Design characteristic |  | Notation | Units | Nominal anchor diameter |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1/4" |  | 3/8" |  | 1/2" |  | 5/8" |  | 3/4" |  |
| Nominal embedment depth |  |  | $\mathrm{h}_{\text {nom }}$ | $\begin{gathered} \mathrm{in}_{(\mathrm{mm})} \end{gathered}$ | $\begin{aligned} & 15 / 8 \\ & (41) \end{aligned}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{aligned} & 41 / 4 \\ & (108) \end{aligned}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & \hline 61 / 4 \\ & (159) \end{aligned}$ |
| Anchor category |  | 1,2 or 3 | - |  |  |  |  |  |  |  |  |  |  |
| STEEL STRENGTH IN TENSION (ACl 318-14 17.4.1 or ACl 318-11 D.5.1) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum specified | ultimate strength | $\mathrm{f}_{\text {uta }}$ | $\begin{array}{\|c\|} \hline \mathrm{psi} \\ \left(\mathrm{~N} / \mathrm{mm}^{2}\right) \\ \hline \end{array}$ |  |  |  |  |  | $000$ |  | $000$ |  |  |
| Minimum specified | yield strength | $\mathrm{fy}_{y}$ | $\begin{gathered} \mathrm{psi} \\ \left(\mathrm{~N} / \mathrm{mm}^{2}\right) \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |  |  |  |
| Effective tensile str body) | ess area (screw anchor | $\mathrm{A}_{\mathrm{se}, \mathrm{N}}$ | $\begin{gathered} \mathrm{in}^{2} \\ \left(\mathrm{~mm}^{2}\right) \end{gathered}$ |  |  |  |  |  |  |  |  |  |  |
| PULLOUT STRENGTH IN TENSION (ACl 318-14 17.4.3 or ACl 318-11 D.5.3) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Characteristic pullo masonry ${ }^{6}$ | ut strength, uncracked | $\mathrm{N}_{\mathrm{p}, \text { uncr }}$ | $\begin{gathered} \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{gathered} 917 \\ (4.08) \end{gathered}$ | $\begin{aligned} & 2167 \\ & (9.64) \end{aligned}$ | $\begin{gathered} \hline 824 \\ (3.66) \end{gathered}$ | $\begin{gathered} \hline 3,953 \\ (17.58) \\ \hline \end{gathered}$ | $\begin{aligned} & 1,633 \\ & (7,26) \end{aligned}$ | $\begin{aligned} & 1,619 \\ & (7.20) \end{aligned}$ | $\begin{gathered} \hline 2,706 \\ (12.04) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 4,513 \\ (20.08) \end{gathered}$ | $\begin{gathered} \hline 3,367 \\ (14.98) \end{gathered}$ | $\begin{gathered} \hline 5,744 \\ (25.55) \\ \hline \end{gathered}$ |
| Characteristic pullo masonry ${ }^{6}$ | ut strength, cracked | $\mathrm{N}_{\mathrm{p}, \mathrm{cr}}$ | $\begin{gathered} \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | -- | -- | $\begin{gathered} 437 \\ (1.94) \\ \hline \end{gathered}$ | $\begin{array}{r} 2,097 \\ (9.33) \\ \hline \end{array}$ | $\begin{gathered} 873 \\ (3.88) \\ \hline \end{gathered}$ | $\begin{gathered} 866 \\ (3.85) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 2,591 \\ (11.53) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 4,321 \\ (19.22) \end{gathered}$ | $\begin{gathered} \hline 2,894 \\ (12.87) \end{gathered}$ | $\begin{gathered} \hline 3,791 \\ (16.86) \end{gathered}$ |
| Characteristic pullo | ut strength, top of wall | $\mathrm{N}_{\text {eq }}$ | $\begin{gathered} \hline \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{gathered} 917 \\ (4.08) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 1,975 \\ & (8.78) \end{aligned}$ | $\begin{gathered} 824 \\ (3.66) \\ \hline \end{gathered}$ | $\begin{array}{r} 1,175 \\ (5.23) \\ \hline \end{array}$ | $\begin{array}{r} 1,485 \\ (6.61) \\ \hline \end{array}$ | $\begin{array}{r} 1,619 \\ (7.20) \\ \hline \end{array}$ | $\begin{array}{r} 1,747 \\ (7.77) \\ \hline \end{array}$ | $\begin{gathered} \hline 3,306 \\ (14.70) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3,303 \\ (14.69) \\ \hline \end{gathered}$ | $\begin{gathered} 4,082 \\ (18.16) \\ \hline \end{gathered}$ |
| Strength reduction in tension ${ }^{4}$ | factor for pullout strength | $\phi_{\text {cb }}$ | - |  |  |  |  |  |  |  |  |  |  |
| Axial stiffness in service load range ${ }^{6}$ | Uncracked masonry | $\beta_{\text {uncr }}$ | $\begin{array}{\|c\|} \hline \mathrm{lb} / \mathrm{in} \\ (\mathrm{kN} / \mathrm{mm}) \end{array}$ | $\begin{aligned} & 105,563 \\ & (18,845) \end{aligned}$ | $\begin{aligned} & 121,349 \\ & (21,252) \end{aligned}$ | $\begin{aligned} & 122.681 \\ & (21,485) \end{aligned}$ | $\begin{aligned} & 121.349 \\ & (21,252) \end{aligned}$ | $\begin{aligned} & 170.136 \\ & (29,795) \end{aligned}$ | $\begin{gathered} 87.954 \\ (15,403) \end{gathered}$ | $\begin{aligned} & 119.675 \\ & (20,958) \end{aligned}$ | $\begin{aligned} & 124.779 \\ & (21,852) \end{aligned}$ | $\begin{aligned} & 110.495 \\ & (19,351) \end{aligned}$ | $\begin{aligned} & 226.287 \\ & (39,629) \end{aligned}$ |
|  | Cracked masonry | $\beta_{\text {cr }}$ | $\mathrm{lb} / \mathrm{in}$ $(\mathrm{kN} / \mathrm{mm})$ | -- | -- | $\begin{aligned} & 144.644 \\ & (25,331) \end{aligned}$ | $\begin{gathered} 76.812 \\ (13,452) \end{gathered}$ | $\begin{gathered} 78.069 \\ (13,672) \\ \hline \end{gathered}$ | $\begin{aligned} & 113.586 \\ & 19,892) \end{aligned}$ | $\begin{gathered} 82.924 \\ (14,522) \end{gathered}$ | $\begin{gathered} 74.917 \\ (13,120) \end{gathered}$ | $\begin{aligned} & 101.211 \\ & (17,725) \end{aligned}$ | $\begin{aligned} & 47.422 \\ & (8,305) \end{aligned}$ |
|  | Top of wall | $\beta_{\text {cr }}$ | $\begin{array}{\|c\|} \hline \mathrm{lb} / \mathrm{in} \\ (\mathrm{kN} / \mathrm{mm}) \end{array}$ | $\begin{gathered} 92,150 \\ (16,138) \end{gathered}$ | $\begin{gathered} 7,993 \\ (1,400) \end{gathered}$ | $\begin{gathered} 93,455 \\ (16,367) \end{gathered}$ | $\begin{aligned} & 47,984 \\ & (8,403) \end{aligned}$ | $\begin{aligned} & 100,955 \\ & (17,680) \end{aligned}$ | $\begin{aligned} & 27,476 \\ & (4,812) \end{aligned}$ | $\begin{aligned} & 41,307 \\ & (7,234) \end{aligned}$ | $\begin{aligned} & 54,810 \\ & (9,599) \end{aligned}$ | $\begin{aligned} & 31,215 \\ & (5,467) \end{aligned}$ | $\begin{gathered} 70,483 \\ (12,344) \end{gathered}$ |
| Coefficient of variation for axial stiffness in service load range | Uncracked masonry | Vuncr | \% | 65 | 33 | 66 | 33 | 55 | 30 | 43 | 57 | 29 | 37 |
|  | Cracked masonry | Vuncr | \% | -- | -- | 62 | 43 | 72 | 47 | 49 | 35 | 45 | 18 |
|  | Top of wall | Vuncr | \% | 37 | 55 | 77 | 22 | 45 | 34 | 44 | 25 | 42 | 51 |

For SI: 1 inch $=25.4 \mathrm{~mm}, 1 \mathrm{in}^{2}=645 \mathrm{~mm}^{2}, 1 \mathrm{psi}=0,00689 \mathrm{~N} / \mathrm{mm}^{2} ; 1 \mathrm{lb}=0,00445 \mathrm{kN}, 1 \mathrm{lbf} / \mathrm{in}=0,175 \mathrm{kN} / \mathrm{mm}$

[^1]
## TDE / TLE

## Shear design information ${ }^{1,2}$

| Design characteristic | Notation | Units | Nominal anchor diameter |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1/4" |  | 3/8" |  | 1/2" |  | 5/8" |  | 3/4" |  |
| Nominal embedment depth | $\mathrm{h}_{\text {nom }}$ | $\begin{gathered} \text { in } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{aligned} & 15 / 8 \\ & (41) \end{aligned}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{gathered} 2 \\ (51) \end{gathered}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 21 / 2 \\ (64) \end{gathered}$ | $\begin{aligned} & 41 / 4 \\ & (108) \end{aligned}$ | $\begin{gathered} 31 / 4 \\ (83) \end{gathered}$ | $\begin{gathered} 5 \\ (127) \end{gathered}$ | $\begin{gathered} 4 \\ (102) \end{gathered}$ | $\begin{aligned} & 61 / 4 \\ & (159) \end{aligned}$ |
| Anchor category | 1, 2 or 3 | - | 1 |  | 1 |  | 1 |  | 1 |  | 2 |  |
| STEEL STRENGTH IN SHEAR (ACl 318-14 17.5.1 or ACl 318-11 D.6.1) ${ }^{5}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum specified ultimate strength | $f_{\text {uta }}$ | $\begin{gathered} \mathrm{psi} \\ \left(\mathrm{~N} / \mathrm{mm}^{2}\right) \end{gathered}$ | $\begin{gathered} 110.000 \\ (758) \end{gathered}$ |  | $\begin{gathered} 111,000 \\ (765) \end{gathered}$ |  | $\begin{gathered} 107,000 \\ (738) \end{gathered}$ |  | $\begin{gathered} 102,000 \\ (703) \end{gathered}$ |  | $\begin{gathered} 99,000 \\ (683) \end{gathered}$ |  |
| Minimum specified yield strength | $\mathrm{fy}_{y}$ | $\begin{gathered} \mathrm{psi} \\ \left(\mathrm{~N} / \mathrm{mm}^{2}\right) \end{gathered}$ | $\begin{gathered} 88.000 \\ (607) \end{gathered}$ |  | $\begin{gathered} 88,800 \\ (612) \end{gathered}$ |  | $\begin{gathered} 85,600 \\ (590) \end{gathered}$ |  | $\begin{gathered} \hline 81,600 \\ (563) \end{gathered}$ |  | $\begin{gathered} 79,200 \\ (546) \end{gathered}$ |  |
| Effective tensile stress area (screw anchor body) | $\mathrm{A}_{\mathrm{se}, \mathrm{V}}$ | $\begin{gathered} \mathrm{in}^{2} \\ \left(\mathrm{~mm}^{2}\right) \end{gathered}$ | $\begin{aligned} & 0.0438 \\ & (28,3) \end{aligned}$ |  | $\begin{aligned} & 0.0943 \\ & (60.8) \end{aligned}$ |  | $\begin{aligned} & 0.1768 \\ & (114.1) \end{aligned}$ |  | $\begin{aligned} & 0.2703 \\ & (174.4) \end{aligned}$ |  | $\begin{aligned} & 0.3988 \\ & (257.3) \end{aligned}$ |  |
| Steel strength in shear, field of wall ${ }^{3}$ | $\mathrm{V}_{\text {sa }}$ | $\begin{gathered} \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{array}{r} 1,959 \\ (8.71) \\ \hline \end{array}$ | $\begin{aligned} & 1,959 \\ & (8.71) \\ & \hline \end{aligned}$ | $\begin{gathered} 3,220 \\ (14.33) \\ \hline \end{gathered}$ | $\begin{array}{\|c} 3,220 \\ (14.33) \\ \hline \end{array}$ | $\begin{gathered} 3,837 \\ (17.07) \end{gathered}$ | $\begin{gathered} 5,524 \\ (24.57) \\ \hline \end{gathered}$ | $\begin{gathered} 6,463 \\ (28.75) \\ \hline \end{gathered}$ | $\begin{gathered} 7,700 \\ (34.25) \end{gathered}$ | $\begin{gathered} 8,973 \\ (39.91) \end{gathered}$ | $\begin{gathered} 9,427 \\ (41.93) \\ \hline \end{gathered}$ |
| Steel strength in shear, top of wall ${ }^{5}$ | $\mathrm{V}_{\text {sa }}$ | $\begin{gathered} \mathrm{lb} \\ (\mathrm{kN}) \end{gathered}$ | $\begin{gathered} 533 \\ (2.37) \end{gathered}$ | $\begin{gathered} 533 \\ (2.37) \end{gathered}$ | $\begin{aligned} & 1,335 \\ & (5.94) \end{aligned}$ | $\begin{aligned} & 1,335 \\ & (5.94) \end{aligned}$ | $\begin{aligned} & 1,991 \\ & (8.86) \\ & \hline \end{aligned}$ | $\begin{aligned} & 1,991 \\ & (8.86) \end{aligned}$ | $\begin{aligned} & 2,175 \\ & (9.67) \end{aligned}$ | $\begin{aligned} & 2,175 \\ & (9.67 \end{aligned}$ | $\begin{gathered} 4,203 \\ (18.70) \\ \hline \end{gathered}$ | $\begin{gathered} 4,203 \\ (18.70) \\ \hline \end{gathered}$ |
| Strength reduction factor for steel failure in shear ${ }^{6}$ | $\phi_{\text {sa }}$ | - | 0.60 |  |  |  |  |  |  |  |  |  |

For SI: 1 inch $=25.4 \mathrm{~mm}, 1 \mathrm{in}^{2}=645 \mathrm{~mm}^{2}, 1 \mathrm{psi}=0,00689 \mathrm{~N} / \mathrm{mm}^{2} ; 1 \mathrm{lb}=0,00445 \mathrm{kN}$

1. The data in this table is intended to be used with the design provisions of ACl 318-14 Chapter 17 or ACl 318 Appendix D, as applicable.
2. Installation must comply with published instructions and details.
3. Reported values for steel strength in shear are based on test results per AC 01 and shall be used for design.
4. All values of $\phi$ were determined from the load combinations of AC01 section 3.3.2.9

## Factored design strength $\left(\Phi N_{n}\right.$ and $\left.\Phi V_{n}\right)$ calculated in accordance with ACl 318-14:

Tabular values are provided for illustration and are applicable for single anchors installed in fully grouted CMU masonry applications:
Edge distances $\mathrm{C}_{\mathrm{a} 1}$ are greater than or equal to the critical edge distance, $\mathrm{C}_{\text {cr }}$.
Calculations were performed according to $\mathrm{ACI} 318-14$ and AC 01.
Strength reduction factors ( $\Phi$ ) were based on AC01 section 3.3.2.9.
Tabular values are permitted for static loads only, seismic loading is not considered with these tables.
For designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318-14 section 17.6.
Interpolation is not permitted to be used with the tabular values. For intermediate base material compressive strengths please see ACl 31814 and AC 01. For other design conditions please see ACI 318-14and AC 01.

## Tension and shear design strengths for TDE / TLE in masonry

| Nominal anchor diameter (in.) | Nominal embed. <br> $h_{\text {nom }}$ <br> (in.) | Uncracked masonry |  |  |  | Cracked masonry |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Field of wall |  | Top of wall |  |  |  |
|  |  | $\Phi \mathrm{N}_{\mathrm{n}}$ Tension (lb.) | $\begin{gathered} \Phi V_{\mathrm{n}} \\ \text { Shear (lb.) } \end{gathered}$ | $\Phi \mathrm{N}_{\mathrm{n}}$ Tension (lb.) | $\Phi V_{n}$ <br> Shear (lb.) | $\begin{gathered} \Phi \mathrm{N}_{\mathrm{n}} \\ \text { Tension (lb.) } \end{gathered}$ | $\Phi V_{n}$ <br> Shear (lb.) |
| 1/4 | $15 / 8$ | 596 | 1,186 | 596 | 323 | -- | -- |
|  | $21 / 2$ | 1,409 | 1,186 | 1,284 | 323 | -- | -- |
| 3/8 | 2 | 536 | 1,932 | 536 | 801 | 284 | 1,932 |
|  | $31 / 4$ | 2,569 | 1,932 | 764 | 801 | 1,363 | 1,932 |
| 1/2 | $21 / 2$ | 1,061 | 2,302 | 965 | 1,195 | 567 | 2,302 |
|  | $41 / 4$ | 1,052 | 3,314 | 1,052 | 1,195 | 563 | 3,314 |
| 5/8 | $31 / 4$ | 1,759 | 3,878 | 1,136 | 1,305 | 1,684 | 3,878 |
|  | 5 | 2,933 | 4,620 | 2,149 | 1,305 | 2,809 | 4,620 |
| 3/4 | 4 | 1,852 | 5,384 | 1,817 | 2,522 | 1,592 | 5,384 |
|  | $61 / 4$ | 3,159 | 5,656 | 2,245 | 2,522 | 2,085 | 5,656 |

## TDE / TLE

## Converted allowable loads for TDE /TLE

ESR-5216 provides design information for load factor and characteristic resistance (LRFD), however allowable stress design (ASD) is still in use by some users. Translation of LRFD to ASD values is possible, however it is dependent on the levels of dead load and live load. Dead load is defined in the ACI 318 Building Code Requirements for Structural Concrete as "the weights of members, supported structure and permanent attachments that are likely to be present on a structure in service". Live load is defined in $\mathrm{ACl} 318-14$ as "load that is not permanently applied to a structure, but is likely to occur during the service life of the structure (excluding environmental loads)". Examples of live loads are traffic on a walkway and non-permanent loads associated with usage of a structure. Live load values are stipulated in the building code for various loading conditions and parts of structures.

To facilitate the translation of LRFD characteristic values to ASD values, a scenario of dead load and live load level is used to conservatively address the most common application as follows: 30\% dead load; 70\% live load. ACI 318-14 Equation (5.3.1b) provides a conversion factor of 1,48 which is divided into the LRFD characteristic resistances and multiplied by a $\phi$ factor (according to the failure type) to determine an equivalent ASD load.

It is the responsibility of the user to select the appropriate ASD values based on the example loadings shown in this document or alternative dead versus live loading that may be applicable to the specific design.

The ASD values are provided in the following tables for tension and shear for different concrete strengths. Other installation and design provisions in ESR-5216 must be followed.

## Converted allowable loads for TDE /TLE in masonry

| Nominal anchor diameter (in.) | Nominal embed. <br> $h_{\text {nom }}$ <br> (in.) | Uncracked masonry |  |  |  | Cracked masonry |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Field of wall |  | Top of wall |  |  |  |
|  |  | $\Phi N_{n}$ | $\Phi \mathrm{V}_{\mathrm{n}}$ | $\boldsymbol{\Phi} \mathrm{N}_{\mathrm{n}}$ | $\Phi \mathrm{V}_{\mathrm{n}}$ | $\Phi N_{n}$ | $\Phi \mathrm{V}_{\mathrm{n}}$ |
|  |  | Tension (lb.) | Shear (lb.) | Tension (lb.) | Shear (lb.) | Tension (lb.) | Shear (lb.) |
| 1/4 | $15 / 8$ | 403 | 801 | 403 | 218 | -- | -- |
|  | $21 / 2$ | 952 | 801 | 867 | 218 | -- | -- |
| 3/8 | 2 | 362 | 1,305 | 362 | 541 | 192 | 1,305 |
|  | $31 / 4$ | 1,736 | 1,305 | 516 | 541 | 921 | 1,305 |
| 1/2 | $21 / 2$ | 717 | 1,556 | 652 | 807 | 383 | 1,556 |
|  | $41 / 4$ | 711 | 2,239 | 711 | 807 | 380 | 2,239 |
| 5/8 | $31 / 4$ | 1,188 | 2,620 | 767 | 882 | 1,138 | 2,620 |
|  | 5 | 1,982 | 3,122 | 1,452 | 882 | 1,898 | 3,122 |
| 3/4 | 4 | 1,251 | 3,638 | 1,227 | 1,704 | 1,075 | 3,638 |
|  | $61 / 4$ | 2,135 | 3,822 | 1,517 | 1,704 | 1,409 | 3,822 |

1. Allowable load values are calculated using a conversion factor, $\alpha$, from factored design strengths.
2. Tabulated allowable load values assume $30 \%$ dead load and $70 \%$ live load, with controlling load combination $1,2 D+1,6 L$. Calculated weighted average for the conversion factor, $\alpha=1,2^{*}(0,3)+1,6^{*}(0,7)=1,48$.

[^0]:    1. Allowable load values are calculated using a conversion factor, $\alpha$, from factored design strengths.
    2. Tabulated allowable load values assume $30 \%$ dead load and $70 \%$ live load, with controlling load combination 1,2D + 1,6L. Calculated weighted average for the conversion factor, $\alpha=1,2^{\star}(0,3)+1,6^{*}(0,7)=1,48$.
[^1]:    1. The data in this table is intended to be used with the design provisions of $\mathrm{ACl} 318-14$ Chapter 17, ACI 318 Appendix D and AC 01 , as applicable.
    2. Installation must comply with published instructions and details.
    3. Tabulated values for steel strength in tension are based on test results per AC01 and must be used for design.
    4. All values of $\phi$ were determined from the load combinations of $A C 01$ section 3.3.2.9.
    5. TDE / TLE screw anchor is considered a brittle steel element in tension as defined by ACI 318-14 2.3 or ACI 318 D.1, as applicable.
    6. Mean values shown; actual stiffness varies considerable depending on loading and geometry of application..
